# DESCRIPTION \& OPERATING INSTRUCTIONS FOR HF COMMUNICATIONS RECEIVER <br> Type CR.Iso/6 

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\text { Technical Handbook }-313 \rightarrow \text { HEAD OFFICE } \\
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Marconi


Receiver Type CR. 150/6


## CONTENTS



## CONTENTS (Contd.)

Page
3.3 Mechanical Construction ..... 6
4 CIRCUIT DESCRIPTION ..... 6
4. 1 General Arrangement ..... 6
4.2 Signal Frequency Circuits
7
7
4.3 Intermediate Frequency Circuits ..... 7
4.4 Third (Beat) Oscillator and Signal Detector
7
7
4.5 Audio Frequency Circuits ..... 7
4.6 Automatic Gain Control Circuits
7
7
4.7 Noise Limiter
8
8
4.8 Crystal Oscillator ..... 8
4.9 Desensitising Circuit
8
8
4. 10 Supply Units ..... 8INSTALLATION9
5.1 For Mains Horking ..... 9
5. 2 For Batteries or from other DC Source
9
9
5.3 Aerial Input Connections
9
9
5.4 Outputs
5.4 Outputs
10
10
5.5 Desensitising Facilities ..... 10
5. 6 AGC Terminals and Time Constant Adjustment ..... 10
5. 7 Diversity Connections ..... 10
6 OPERATING INSTRUCTIONS ..... 11
6. 1 General ..... 11
6.1.1 Preliminary Adjustments ..... 11
6.1.2 Use of PASSBAND Switch ..... 11
6.1.3 Use of AGC ..... 11
6.1.4 Use of Gain Controls ..... 12
6.1.5 Use of Calibration
12
12
6.1.6 Use of Meter as Tuning Indicator ..... 12
6.1.7 Use of Noise Limiter ..... 12
6.1.8 Use of Logging Scale ..... 12
6.1.9 Use of Crystal Controlled First Oscillator ..... 13
6.1. 10 Adjustment of Third Oscillator ..... 13
6.1.11 Warming Up ..... 14
7 MAINTENANCE ..... 14
7. 1 General ..... 14
7. 2 Routine Maintenance ..... 14
7.2.1 Valve Replacements ..... 14
7.2.2 Replacing the Calibration Drum Drive Cord ..... 15
7.2.3 Replacing the Pointer Drive Cord ..... 16
7. 3 Circuit Checks ..... 16
7.4 Voltages and Feeds ..... 16

## CONTENTS (Contd.)

Page
7.4.1 Power Consumption ..... 17
7.4.2 Voltages ..... 17
7.4.3 Valve Feeds ..... 17
7.4.3.1 Metered Feeds ..... 17
7.4.3.2 Feeds to V7 and V8 ..... 18
7.4.3.3 Feed to V9 ..... 18
7.4.3.4 Current through Stabiliser Tube V14 ..... 19
7.5 Receiver Alignment ..... 19
7.5.1 Test Equipment ..... 19
7.5.2 AF Amplifier Tests ..... 19
7.5.2.1 Sensitivity ..... 20
7.5.2.2 AF Anplifier Tests ..... 20
7.5.3 Alignment of $465 \mathrm{kc} / \mathrm{s}$ IF Amplifier Circuits ..... 20
7.5.3.1 General ..... 20
7.5.3.2 Controls ..... 20
7.5.3.3 Tuning IFT. 4, IFT. 5 and IFT 6 (without alignment oscilloscope) ..... 20
7.5.3.4 Tuning IFT.4, IFT.5 and IFT 6 (with alignment oscilloscope) ..... 21
7.5.3.5 Third Oscillator, Tuning and Output Voltage ..... 22
7.5.3.6 Tuning IFT. 2 and IFT. 3 (without alignment oscilloscope) ..... 22
7.5.3.7 Tuning IFT. 2 and IFT. 3 (with alignment oscilloscope) ..... 23
7.5.3.8 Capacitance Trimmers C47, C124, C57 and C126 ..... 23
7.5.3.9 Retuning IFT. 6 (after using alignment oscilloscope) ..... 23
7.5.4 Second Oscillator, Tuning and Output Voltage ..... 23
7.5.5 Selectivity of $465 \mathrm{kc} / \mathrm{s}$ IF Amplifier ..... 24
7.5.6 Stage Gains of $465 \mathrm{kc} / \mathrm{s}$ IF Amplifier ..... 24
7.5.7 Variation of Gain with Bandwidth ..... 25
$7.5 .8 \quad 1600 \mathrm{kc} / \mathrm{s}$ IF Amplifier ..... 25
7.5.8.1 IF. 1 Response ..... 26
7.5.8.2 Retuning IFT. 1 ..... 26
7.5.8.3 IF. 1 Gain ..... 26
7.5.9 Signal Frequency Amplifier ..... 27
7.5.9.1 First Oscillator Alignment ..... 27
7.5.9.2 Alignment of Signal Frequency Circuits ..... 27
7.5. 10 First Oscillator Voltages ..... 28
7.5.10.1 Variable LC Oscillator ..... 28
7.5.10.2 Crystal Oscillator ..... 28
7.5.10.3 External Oscillator ..... 29
7. 6 Overall Performance ..... 29
7.6.1 CW Sensitivity ..... 29
7. 6.2 Sensitivity for Modulated Signals ..... 29
7.6.3 AGC ..... 30

## CONTENTS (Contd.)



## LIST OF ILLUSTRATIONS

Frontispiece

Number
29512

## Miscellaneous

Block Diagram
Logging Scale
Method of Fixing Aerial Feeder Cable to Plug
Cord Drive Assembly
CIrcuit diagram and component layout diagrams
Circuit Diagram of Receiver
Component Layout of Recefver
Circuit Diagram of Supply Unit
Component Layout of Supply Unit
PERFORMANCE CURVES
IF Response
AF Response
Overall Frequency Response
AGC Characteristic
Frequency Drift
Electric Shock Treatment
(WZ. 10602/B Sh. 1) Fig. 2
(HZ. 10953/C Sh. 1)
Fig. 3
Fig. 4
(MSK. 13976 Sh. I) Fig. 5

| (WZ. 8394/D | Sh. 1) | Fig. 6 |
| :--- | :--- | :--- |
| (WZ. 8395/D | Sh. 1) | Fig. 7 |
| (HZ. $4768 /$ B | Sh. 1) | Fig. 8 |
| (WZ. 10728/B Sh.1) | Fig. 9 |  |

(HZ. 10604/B Sh. 1) Fig. 10
(HZ. 10606/B Sh. 1) Fig. 11
( HZ 10607/B Sh.1) Fig. 12
(HZ. 10605/B Sh. 1) Fig. 13
(HZ. 10603/B Sh. 1) Fig. 14
(WZ. 12308/B Sh.1)

# DESCRIPTION \& OPERATING INSTRUCTIONS FOR HF COMMUNICATIONS RECEIVER TYPE CR.150/6 

## 1 INTRODUCTION

## 1. 1 GENERAL

The CR150/6 receiver shown in the Frontispiece (Fig. 1) is a modified version of the CR150/3 and covers the range 2 to $32 \mathrm{Mc} / \mathrm{s}$ in four bands. The receiver is a double-superheterodyne employing intermediate frequencies of $1600 \mathrm{kc} / \mathrm{s}$ and $465 \mathrm{kc} / \mathrm{s}$. A crystal-controlled first oscillator operating on six spot frequencies is incorporated in addition to the variable LC-controlled oscillator. Four pass-bands of $1,3,8$ and $13 \mathrm{kc} / \mathrm{s}$ are provided. All valves used in the receiver are British Services preferred types. There are three models of the CR150/6 receiver; Edition A for table mounting is shown in the Frontispiece (Fig. 1); Edition B is similar but is suitable for rack mounting, and Edition $C$ which is supplied without a cover and is intended for mounting in a cabinet.

To reduce temperature changes in the receiver, the power supply unit is contained in a separate case which may be placed beside the receiver or in any other convenient position. There are two similar types of Supply Unit; the Type $1325 / 4$ for table mounting and the Type 1325/5 for Rack or Cabinet mounting. Electrically, the receivers are identical and so are the Supply Units. The dimensions and weights of the receiver and supply unit are given in Table 1.

TABLE 1

| Unit | width | Depth | Height | Weight |
| :---: | :---: | :---: | :---: | :---: |
| Receiver Unit Type CR150/6 | $20.5 i n$. <br> $(52 \mathrm{~cm})$ | 17 in. <br> $(43 \mathrm{~cm})$ | 14 in. <br> $(35.6 \mathrm{~cm})$ | 16 lb. <br> $(28 \mathrm{~kg})$ |
| Supply Units Type $1325 / 4$ | $5.25 i n$. <br> $(13.3 \mathrm{~cm})$ | 15 in. <br> $(38 \mathrm{~cm})$ | 12 in. <br> $(30.5 \mathrm{~cm})$ | 25 lb. <br> $(11.3 \mathrm{~kg})$ |

## 2 TECHNICAL SUMMARY

## 2. 1 SALIENT FEATURES

### 2.1.1 Types of Service

The receiver is designed for the reception of $\mathrm{CW}, \mathrm{MCW}$ or telephony transmissions and covers the range $2 \mathrm{Mc} / \mathrm{s}$ to $32 \mathrm{Mc} / \mathrm{s}$ ( 150 to 9.4 metres) in four bands. If desired, diversity reception may be employed by using two or more receivers. For this purpose, comections are provided on the receiver for an external common oscillator and for a common automatic gain control circuit.

### 2.1.2 RF Input

The aerial may be connected directly to the receiver or via a 75-100 ohm balanced or unbalanced feeder.

### 2.1.3 AF Output

Output connections for a 3 ohm Ioudspeaker, high or low resistance phones and a 600 ohm line are provided.

### 2.1.4 Tropical Use

The receiver is suitable for continuous operation under tropical conditions.

### 2.1.5 Power Supplies

The receiver supply unit Type $1325 / 4$ or $1325 / 5$ will operate from a single-phase $50-60 \mathrm{c} / \mathrm{s} \mathrm{AC}$ source of 200 to 250 volts, or the receiver alone may be operated from batteries.

### 2.2 ELECTRICAL CHARACTERISTICS

### 2.2.1 Circuit Details

The receiver employs a double superheterodyne circuit with a first IF of $1600 \mathrm{kc} / \mathrm{s}$ and second IF of $465 \mathrm{kc} / \mathrm{s}$. Two signal frequency amplifiers and an amplifier at the first IF are followed by three amplifiers at the second IF incorporating the main selective circuits. The detector is followed by a noise limiter and two stages of audio-frequency amplification. A block diagram is given in Fig. 2.

### 2.2.2 Selectivity

High discrimination against adjacent channel interference is obtained by the use of band-pass crystal filters at $465 \mathrm{kc} / \mathrm{s}$. Four pass-bands of $1,3,8$ and $13 \mathrm{kc} / \mathrm{s}$ are provided so that the selectivity may be adjusted to suit the conditions of service. High discrimination against image response is obtained by using a relatively high first intermediate frequency ( $1600 \mathrm{kc} / \mathrm{s}$ ).

### 2.2.3 Sensitivity

The sensitivity is good on all ranges and is limited only by the noise level inherent in the first RF stage.

### 2.2.4 Automatic Gain Control (AGC)

The automatic gain control circuits enable wide fluctuations of signal strength to be tolerated; alternative time constants are provided to suit the type of signal being received.

### 2.2.5 Crystal Control

The first oscillator may be crystal-controlled on any six spot frequencies.

## 2. 2. 6 Desensitising

A desensitising circuit enables the receiver to be fully or partially muted during transmission.

### 2.2.7 Metering

A meter, in conjunction with a selector switch, may be used to measure anode feeds or act as a tuning indicator.

### 2.3 TUNING

### 2.3.1 Frequency Selection

A single tuning control with fast or slow motion is employed and provides continuous coverage of each frequency band. The main tuning scale is calibrated directly in signal frequencies and there is also an auxiliary logging-scale with high discrimination. All receivers are individually calibrated.

### 2.3.2 Fine Tuning

A fine-tuning control operating on the second local oscillator covers the range $\pm 4 \mathrm{kc} / \mathrm{s}$ at all signal frequencies.

### 2.3.3 Crystal Calibrator

A crystal-controlled calibrator oscillator is incorporated in the receiver. This oscillator provides check frequencies at intervals of $500 \mathrm{kc} / \mathrm{s}$ so that the frequency calibration of the main tuning scale may be checked; also, by interpolating on the logging scale between two check frequencies, the receiver may be tuned exactly to any desired frequency.

### 2.4 PERFORMANCE

### 2.4.1 Sensitivity

The receiver sensitivity is expressed in Table 2 as the input voltage in series with 75 ohms required to give a 20 db signal-to-noise ratio on an unmodulated signal, or a 10 db signal-to-noise ratio on a signal modulated $40 \%$ at $400 \mathrm{c} / \mathrm{s}$. The passband switch is set at $8 \mathrm{kc} / \mathrm{s}$.

TABLE 2

| Wave <br> Band | Frequency Range <br> in Mc/s | Sensitivity <br> (db rel. $1 \mu$ ) | Image signal <br> Protection | Frequency Drift <br> per hour, <br> than. | Noises <br> Factor. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 to 4 | +3 to +5 db | $110-90 \mathrm{db}$ | $0.01 \%$ | +3 to +5db |
| 2 | 4 to 8 | +3 to +5 db | $110-90 \mathrm{db}$ | $0.01 \%$ | +3 to +5db |
| 3 | 8 to 16 | +3 to +5 db | $100-70 \mathrm{db}$ | $0.01 \%$ | +3 to +5db |
| 4 | 16 to 32 | +5 to +9 db | $85-50 \mathrm{db}$ | $0.02 \%$ | +5 to +9db |

### 2.4.2 Selectivity

The amount by which the image signal is attenuated is shown in column 4 of Table 2.

The adjacent-channel selectivity expressed as bandwidth at 6 db and 40 db attenuation is shown in Table 3. IF response curves are shown in Fig. 10 ( $\mathrm{HZ} .10604 / \mathrm{B}$ Sh. 1).

TABLE 3

| Passband switch <br> set at | 日andwidth in c/s |  |
| :---: | ---: | ---: |
|  | -6 db | -40 dD |
| $1 \mathrm{kc} / \mathrm{s}$ | 1000 | 4000 |
| $3 \mathrm{kc} / \mathrm{s}$ | 3000 | 8500 |
| $8 \mathrm{kc} / \mathrm{s}$ | 8000 | 18000 |
| $13 \mathrm{kc} / \mathrm{s}$ | 13000 | 30000 |

### 2.4.3 Fidelity

The overall frequency response curves for the $8 \mathrm{kc} / \mathrm{s}$ and $13 \mathrm{kc} / \mathrm{s}$ passbands are shown in Fig. 12 (WZ. 10607/B Sh.1). Response curve for the audio frequency stages is shown in Fig. 11 (HZ. 10606/B Sh.1).

### 2.4.4 Thermal Stability

The frequency drift at any signal frequency up to $30 \mathrm{Mc} / \mathrm{s}$ is less than $5 \mathrm{kc} / \mathrm{s}$ per hour after 30 minutes from switching on.

### 2.4.5 Automatic Gain Control

The output of the receiver does not increase by more than 10 db when the input signal is increased to 60db above the levels specified in column 2 (Sensitivity) of Table 2. The AGC time constant may be selected to suit the type of signal being received.

### 2.4.6 Outputs

The receiver provides three separate outputs as follows:-
1 mW to high or low resistance headphones.
20 mW to 600 ohm line.
100 mW to 3 ohm loudspeaker.

### 2.4.7 Power Consumption

Mains operation:
60 watts (approximately)
Battery operation:
65 mA at $280 \mathrm{~V} ; 3.7 \mathrm{~A}$ at $6,3 \mathrm{~V}$.

## 3 GENERAL DESCRIPTION

## 3. 1 CONTROLS

The receiver controls are as follows:-

### 3.1.1 Power Supply Switch

The power supplies for the receiver are normally switched on or off by the MAINS switch on the Supply Unit Type 1325/4 or 1325/5.

### 3.1.2 Band Change Switch

Any one of the four bands may be selected by the band change switch on the front of the receiver (SWA in WZ. 8395/D Sh.1). When this switch is operated the appropriate frequency scale is automatically displayed on the calibrated drum.

### 3.1.3 Taning Controls

Each receiver is individually calibrated during factory tests; the main tuning scale is calibrated to show the frequency directly in Mc/s. The main tuning control rotates the ganged variable capacitors C119 - C122, moves the pointer across the frequency scale and rotates the logging scale discs. The logging scale has an equivalent length of 18 feet and its 1250 divisions may be read to one quarter division. At $20 \mathrm{Mc} / \mathrm{s}$ one scale division corresponds to a $12 \mathrm{kc} / \mathrm{s}$ change of frequency. The fine tuning control operates on the second oscillator and enables a change of frequency of up to $\pm 4 \mathrm{kc} / \mathrm{s}$ to be made at any frequency in the range. The control is normally set to centre zero.

### 3.1.4 Selectivity Control

The PASS-BAND switch introduces crystal or LC filters into the IF circuits and enables pass-bands of $1,3,8$ or $13 \mathrm{kc} / \mathrm{s}$ to be selected.

### 3.1.5 Operational Switch

This switch has four separate functions:-
(a) Switches the AGC on or off.
(b) Switches the third oscillator on for CW reception.
(c) Switches on the calibration checking oscillator when required.
(d) Switches off the noise limiter in position 2.

### 3.1.6 Gain Controls

The HF GAIN control rotates the ganged potentiometers RV94 and RV93 in the cathode circuits of the RF and IF stages.

The AF GAIN control rotates the potentiometer RV92 in the grid circuit of the first AF amplifier V7.

### 3.1.7 Meter Switch

This switch enables individual valve feeds to be checked as described in Section 7.4.3. The meter may also be used as a tuning indicator.

## 3. 1.8 Preset Controls

Access to the receiver desensitising control tayy be obtained by moving to one side the small cover plate on the front panel. The adjustment of this and other preset controls, including the signal-indicator zero setting and the third oscillator frequency, is described in Section 6.

### 3.2 LOCATION OF COMPONENTS

The position of each component in the receiver is shown in WZ. 8395/D Sh. 1. A label attached to the inside of the hinged cover lists the valve types and their positions in the receiver.

## 3. 3 mechanical construction

The receiver components are mounted on a chassis which is housed in a steel case with a hinged lid so that valves and crystals may be changed and internal adjustments may be made without removing the chassis from its case. To withdraw the receiver for servicing it is necessary only to remove four screws from the front panel.

The receiver chassis is of the inverted tray type with the valves, IF transformers, main tuning capacitors and certain other components mounted on the upper deck and the control switches, fixed capacitors and resistors mounted underneath the deck. The RF circuits are included in a sub-assembly which is insulated from the main chassis to reduce the possibility of coupling between the signal-frequency circuits and the second and third oscillators.

## 4 CIRCUIT DESCRIPTION

### 4.1 GENERAL ARRANGEMENT

A block diagram of the receiver is shown in Fig. 2 (WZ. 10602/B Sh. 1) and the circuit diagram is given in Fig. 6 ( $\mathrm{HZ} .8394 / \mathrm{D}$ Sh. 1). The receiver employs two stages of signal frequency amplification followed by a heptode mixer with separate first frequency-change oscillator. The first intermediate frequency is $1600 \mathrm{kc} / \mathrm{s}$ and the first mixer is coupled directly to the second mixer via a pair of coupled circuits tuned to this frequency. The second mixer is a heptode with separate second frequency change oscillator: the output at the second intermediate frequency of $465 \mathrm{kc} / \mathrm{s}$ which is passed through a two-stage amplifier incorporating the main selective cfrcuits and bandpass crystal filters. The $465 \mathrm{kc} / \mathrm{s}$ IF output is rectified by the two diodes of a double-diode triode; one diode provides an audio frequency output while the output from the other is used for AGC. The triode section of this valve functions as the first audio frequency amplifier and is followed by a triode output stage. The beat oscillator is coupled to the signal diode.

## 4. 2 Signal frequency clrcuits

The aerial input is taken to two coaxial sockets which are connected to the low impedance winding of the first RF transformer. The signal frequency circuits are designed to minimise the variation of gain with frequency. The first oscillator assembly is robustly constructed and has good mechanical and thermal stability; this oscillator may be crystal-controlled for reception on any six selected frequencies between $2 \mathrm{Mc} / \mathrm{s}$ and $32 \mathrm{Mc} / \mathrm{s}$.

### 4.3 INTERMEDIATE FREQUENCY CIRCUITS

The first IF transformer is mounted on the RF sub-assembly and the output at $1600 \mathrm{kc} / \mathrm{s}$ is passed to the second mixer valve on the main receiver chassis. The second mixer is a heptode with a separate oscillator operating at a frequency of $1135 \mathrm{kc} / \mathrm{s}$. This oscillator is provided with a FINE TUNING control on the front panel which enables a change of $4 \mathrm{kc} / \mathrm{s}$ to be made on each side of the centre zero so that the receiver may be tuned across the selectivity curve of the signal frequency and first intermediate frequency circuits; these circuits are designed so that mistuning by the FINE TUNING control does not cause more than one decibel of asymmetry at the worst point.

The second IF amplifier ( $465 \mathrm{kc} / \mathrm{s}$ ) controls the overall selectivity of the receiver; the two widest passbands are determined by variation of coupling between two pairs of tuned circuits. One double crystal filter is introduced for the $3000 \mathrm{c} / \mathrm{s}$ passband and a second double crystal filter reduces the passband to $1000 \mathrm{c} / \mathrm{s}$.

### 4.4 THIRD (BEAT) OSCILLATOR AND SIGNAL DETECTOR

The beat oscillator V13 is capacitance-coupled to the signal diode V7a which is supplied with the second IF at $465 \mathrm{kc} / \mathrm{s}$ from the secondary of the last intermediate frequency transformer IFT6. The amplitude of the beat oscillator voltage is such that, although it will fully modulate the strongest signal, it will not operate the automatic gain control. Efficient screening is employed to prevent harmonics from the beat oscillator circuits from interfering appreciably with the signal-frequency input.

### 4.5 AUDIO FREqUENCY CIRCUITS

The triode elements in V7 function as an audio-frequency amplifier which is resistance-capacitance coupled to the output valve v8 which provides outputs for headphones at jacks JKA and JKB and outputs for a 600 ohm line and for a 3 ohm loudspeaker at the secondaries of the output transformer TR1.

## 4. 6 automatic gain control cibcuits

The input to the automatic gain control diode $V 7 b$ is taken from the primary of the last intermediate frequency transformer IFT6 via the capacitor C64. The full AGC voltage is applied to the second mixer valve and first IF amplifier and approximately one sixth of the AGC voltage is applies to the two signal-frequency amplifiers. A choice of two AGC time constants is available by using a selector board inside the receiver. This facility is required for high-speed recording applications.

The automatic gain control may be switched in or out by the operational switch on the front panel. This switch has seven positions which include the following:-
(a) Standby
(b) Third oscillator ON (with and without AGC)
(c) Third oscillator OFF (with and without AGC and noise limiter)
(d) Crystal calibrator.

### 4.7 NOISE LIMITER

The double-diode elements of $v 9$ operate in an impulse noise-limiting circuit. The "series" diode at Pin 6 is in series with the two resistors R50 and R47 and is connected across the resistor $R 48$ which is part of the detector load. This diode is normally conducting in the presence of a signal since its anode is at a positive potential relative to the cathode. When in this condition, the audio-frequency potential developed at the cathode is passed to the control grid of the first AF amplifier, the triode section of V7. The junction of R50 and R47 is held at earth potential to AF signals by the capacitor C72 and the time constants of the circuit are such that a noise impulse of short duration, equivalent to more than $100 \%$ modulation of the signal being received, will cause the anode potentiel of vg (pin 6) to drop instantaneously to a value lower than that of its cathode and, therefore, the diode will cease to conduct.

Additional protection is afforded by the action of the "shunt" diode v9 (pin 5) which by-passes to earth through C72 any excessive noise impulse which may appear at the anode before the "series" diode has ceased to conduct.

### 4.8 CRyStal CAlibrator

The triode elements of v9 may be switched to work as a crystal-controlled oscillator, the frequency being controlled by an AT - cut crystal of low temperature - coefficient. The oscillator circuits are dimensioned to provide strong harmonics of the fundamental $500 \mathrm{kc} / \mathrm{s}$ oscillations and its output is coupled $v i a$ the capacitor C83 to the second tuned circuit of the receiver. The amplitude of these harmonics is sufficient for checking the receiver calibration at any multiple of $500 \mathrm{kc} / \mathrm{s} u p$ to $32 \mathrm{Mc} / \mathrm{s}$.

## 4.9 desensitisine circuit

The cathode bias to the RF and IF stages can be increased by introducing a variable resistor RV95 between earth and the gain control potentiometers. Terminals marked DESENSITISING on the terminal board enable this resistor to be connected to the keying relay or to back contacts on the transmitting key. The receiver may thus be fully or partially muted during transmission.

## 4. 10 SUPPLY UNITS

For operating the receiver from an $A C$ source, the Supply Units Type $1325 / 4$ and Type 1325/5 are provided. The two types are identical electrically, each employing a metal rectifier and paper dielectric capacitors. The Type $1325 / 4$ is intended for table mounting and the 1325/5 for rack or cabinet mountings.

The circuit diagram Fig. 8 shows that the mains are connected to a two pin plug from which connections are made via the ON/OFF switch and 2-amp mains fuses to the transformer primary. Tappings are provided for any standard supply voltage in the 110 volt or 220 volt range. An HT fuse, rated at 500 mA , is connected between the centre tap on the HT secondary and earth. The 280 volt DC and 6.3 volt AC outputs are connected to a $5-$ pin socket mounted at the back of the chassis. A connector cord and plug convey the supplies to the receiver.

The inputs and outputs of the Supply Units are as follows: -
Input $200-250$ volts, 50 to $60 \mathrm{c} / \mathrm{s}$ single-phese $A C$.
(Tappings at $100,215,230$ and 250 volts permit adjustments to suit available mains voltages).

Outputs 280 volts DC at 65 mA .
6.3 volts $A C$ at 4 amps.

Consumption 60 watts.

## 5 INSTALLATION

### 5.1 FOR MAINS mORKING

The Supply Unit should be connected to the receiver by the connector cable terminated by a 7 pin socket. It is important to check that the primary taps on the mains transformer in the Supply Unit are set to suit the supply voltage before switching on the mains. The mains should be connected to the Supply Unit by means of a 3 -core cable fitted with a 5 -anp plug.

## 5. 2 FOR BATTERIES OR FROM OTHER DC SOURCE

The Supply Unit is not required when the receiver is to be operated from a DC source. The DC supplies should be brought to the $7-\mathrm{pin}$ plug on the receiver as follows: -

Pins 1 and 7 to LT 6.3 volts
Pins 2 and 3 to LT earth
Pin 4 to $H T$ positive

Pin 5 to HT earth
Protective fuses should be connected in the supply lines,

## 5.3 aERIAL INPUT CONNECTIONS

Two coaxial input sockets are located at the back of the receiver for a balanced input 75 to 100 ohms. For an unbalanced input from a single coaxial feeder, one socket only is used and the inner and outer conductors of the other socket are connected together. With the same arrangement direct connection may be made to an aerial.

### 5.4 OUTPUTS

Terminals marked LS and LINE located on the rear of the receiver chassis are provided for connection to a 3 -ohm loudspeaker and a 600 ohm line respectively.

Two telephone jacks mounted on the front panel are for use with either high or low resistance headphones; two pairs of headphones may be used simultaneously but one high and one low resistance pair connected in parallel will not give satisfactory results.

### 5.5 DESENSITISING FACILITIES

In a combined transmitting and receiving installation it may be necessary to mute the receiver during transmissions. For this purpose two terminals marked DESENSITISING are provided at the back of the receiver and are normally strapped together. When muting is employed the shorting link should be removed and the terminal connected by a screened pair of leads to the transmitter keying relay, or back contacts on the transmitting key.

When the transmitter key is pressed the RF and IF Cathode bias in the receiver is increased by introducing all or part of an additional 2500 ohm variable resistor RV95 at the earthy end of the RF and IF gain controls RV94 and RV93.

By moving the cover marked $D$ on the front panel the potentiometer RV95 mounted above the HF GAIN control may be adjusted by a screwdriver so that the operator hears the transmitter at a convenient level.

## 5.6 agC terminals and time constant adjustment

For normal operation the AGC terminals 1 and 2 at the rear of the receiver should be strapped together. The AGC time constant adjustment consists of a two-pin connecting link and a small insulated panel with three pin sockets mounted immediately to the right of V7 and V13 on the top deck of the receiver chassis.

The position marked $0.5 \mu \mathrm{~F}$ gives a time constant of approximately 0.2 secs. for the MOD. position and 1.75 secs. for the $C W$ position of the operational switch; this position should be used for normal working.

The position marked $0.1 \mu F$ gives a time constant of approximately 0.5 secs. for the CW and the MOD. positions of the operational switch; this position should be used for high-speed recording when the receiver is used with a Type HU. 11 or other similar type of Recording Unit.

## 5. 7 DIVERSITY CONNECTIONS

When a receiver forms part of a diversity equipment the plug marked EXT. OSC. at the back of the receiver chassis, is used to enable two or more receivers to be supplied from an external common first oscillator; when thus employed, the first oscillator selector switch (SWE) on the front panel should be set to EXT. OSC. The input required from the external oscillator is approximately 1 volt into 68 ohms).

An output at $465 \mathrm{kc} / \mathrm{s}$ is provided for use when an IF operated unit is employed in conjunction with the receiver.

The AGC terminals 1 and 2 should be strapped together and connected to the AGC terminals on the other receiver.

## 6 OPERATING INSTRUCTIONS

### 6.1 GENERAL

Assuming that the installation has been carried out in accordance with Section 5 , the receiver may be switched on and set up for reception on the appropriate signal frequency. The sequence of operations for tuning the receiver and the use of the various controls are as follows:-

### 6.1.1 Preliminary Adjustments

(a) Switch on AC MAINS and switch on Supply Unit. The pilot lamp and scale illuminating lamps should light.
(b) Set operational switch to CW/MAN.
(c) Set passband switch to $3 \mathrm{kc} / \mathrm{s}$.
(d) Set AF GAIN control to mid-position.
(e) Set HF GAIN control to maximum (fully clockwise), reducing if necessary to give comfortable level in headphones.
(f) Set BAND-CHANGE switch to frequency band required. The frequency calibration for each band is automatically brought into view on the calibration drum as the BAND-CHANGE switch is operated.
(g) Set the pointer on the calibration scale to the desired frequency by turning the larger tuning knob, and locate the wanted signal by using the small knob. If telephony is to be received, set the operation switch to MOD/MAN. and re-tune slightly. Reduce the signal to a suitable level by turning the HF gain control counter-clockwise.
(h) During short stand-by periods the HT supply to certain valves may be cut off by turning the operational switch to the OFF position.

### 6.1.2 Ube of PASS bAND Switch

The $13 \mathrm{kc} / \mathrm{s}$ passband gives best intelligibility for reception of speech and also makes the tuning broader, but this passband may be used only when little interference is present. As the passband is narrowed by switching from $8 \mathrm{kc} / \mathrm{s}$ to $3 \mathrm{kc} / \mathrm{s}$ and then to $1 \mathrm{kc} / \mathrm{s}$, interference will be cut down progressively but the signal must be tuned in more carefully and accurately.

NOTE: - When receiving CW with the passband switch at $13 \mathrm{kc} / \mathrm{s}$ or $8 \mathrm{kc} / \mathrm{s}$, it will be found that on tuning through zero beat, the beat note obtained is equally strong on both sides of zero, but when using the $3 \mathrm{kc} / \mathrm{s}$ or $1 \mathrm{kc} / \mathrm{s}$ passband the beat note will be stronger on one side than the other. Always tune to the stronger of the two.

### 6.1.3 Use of AtC

AGC should be switched off (operational switch to MAN. position) when searching or when strong interference is present.

### 6.1.4 Use of Gain Controls

(a) With AGC on, set HF GAIN to maximum and AF GAIN as desired.
(b) With AGC off, set HF GAIN as desired and AF GAIN to approximately midposition

### 6.1.5 Use of Calibrator

When the operational switch is set to the CALIBRATE position, a $500 \mathrm{kc} / \mathrm{s}$ oscillator is switched on and a calibrating signal may be heard every $500 \mathrm{kc} / \mathrm{s}$ up to $32 \mathrm{mc} / \mathrm{s}$.

### 6.1.6 Use of Meter as Tuning Indicator

When the FEEDS switch (SWD) is set to the SIGNAL INDICATOR position the meter may be used as a tuning indicator. Before using the meter in this way, it must be set to give zero reading in the absence of a signal as follows:-
(a) Set the operational switch to MOD-AGC and the HF GAIN control nearly to maximum.
(b) Adjust the tuning control to a silent point.
(c) Adjust the SIGNAL INDICATOR ZERO control, which is mounted on the chassis deck until zero reading is obtained.

With the meter switch set to the other positions the valve feeds of V1 to V6 and V10 to V13 may be measured; with the HF GAIN control at maximum these feeds should be within the limits specified in Table 8.

### 6.1.7 Use of Noise Limiter

The noise limiter is operative for all receiving positions of the operational switch except position 2 (MOD. AGC, NL. OFF).

The noise limiter does, however, introduce some unavoidable distortion of modulation peaks, and so when receiving transmissions of high quality, music or speech, it should be switched off by setting the operational switch to position 2.

### 6.1.8 Use of Logging Scale

This scale enables the operator to reset the receiver accurately to a station that has been received previously. Some slight allowance for initial frequency drift should be made if the receiver has been switched on for less than 30 minutes.

Read the scale divisions from right to left, main divisions on the upper scale and sub-divisions on the lower scale. Note that the scale reading increases as the frequency is increased.

The approximate discrimination of the scale at the lowest, middle and highest frequency in each band is given in Table 4.

TABLE 4

| Switch <br> Position | $\mathrm{kc} / \mathrm{s}$ per small division (0.02) |  |  |
| :---: | :---: | :---: | :---: |
|  | Lowest | Middle | Highest |
| Band 1 | 1 | 2 | 2.5 |
| Band 2 | 2 | 4 | 5 |
| Band 3 | 4 | 8 | 10 |
| Band 4 | 8 | 16 | 20 |

## 6. 1.9 Use of Crystal Controlled First Oscillator

The receiver may be crystal controlled on six selected frequencies by setting the first oscillator selector switch to the appropriate crystal position and setting the band switch and main tuning control to the required signal frequency; the tuning should then be adjusted for maximum signal output. Holders are provided for six crystals.

The crystal frequency required for any specific signal frequency may be calculated as follows:-

For Bands 1, 2 and 3, crystal frequency $=($ signal frequency $+1600 \mathrm{kc} / \mathrm{s})$.
For Band 4, crystal frequency $=1 / 2$ (signal frequency $+1600 \mathrm{kc} / \mathrm{s}$ ).
NOTE: - Hhen ordering crystals it is essential to specify the signal frequency required and not the crystal frequency

## 6. 1. 10 Adjustment of Third 0scillator

The preset tuning capacitor for the third oscillator must be set correctly in the first instance and checked periodically to make the best use of the high selectivity of the receiver when it is switched to the $1 \mathrm{kc} / \mathrm{s}$ passband.

The capacitor, C102, is adjusted by means of a knob on the top of the screening box containing the third oscillator circuit. Three setting marks indicate approximately the positions for $1000 \mathrm{c} / \mathrm{s}$ above the IF , zero beat, and $1000 \mathrm{c} / \mathrm{s}$ below the IF .

The adjustment of this control should be checked as follows: -
(a) Set the passband switch to $1 \mathrm{kc} / \mathrm{s}$.
(b) Set the BANDCHANGE switch to BAND 1.
(c) Tune to any silent point.
(d) Adjust Cl02 until the receiver noise level reaches maximum.

### 6.1.11 Barming Up

The receiver takes a few minutes to warm up and about 30 minutes to reach stability. The operational switch should be turned to OFF during short breaks as the val ve heaters are left on and the receiver is ready for immediate use.

## 6. 1. 11 Tarming Up

The receiver takes a few minutes to warm up and about 30 minutes to reach stability. The operational switch should be turned to OFF during short breaks as the valve heaters are left on and the receiver is ready for immediate use.

## 7 MAINTENANCE

## 7. I GENERAL

This Section covers the routine maintenance and complete realignment of the receiver using standard test equipment usually available.

- It is strongly emphasised that random adjustments to trimmer capacitors or other preset controls should never be undertaken; any necessary adjustments to these controls should be made only by staff having appropriate experience and with suitable test equipment available.


## 7.2 nOUTINE MAINTENANCE

To avoid the accumulation of dust on the components and controls the receiver lid should always be kept closed except when making internal adjustments. It is desirable to lubricate occasionally the click register and bandchange mechanisms with a Iight machine oil of good quality; when lubricating it is essential to avoid applying any trace of oil to the switch wafers or other electrical contacts and keep the units reasonably clean.

If it becomes necessary to remove dust or other matter from the main tuning capacitor, a pipe-cleaner or feather should be carefully inserted between the plates.

Always switch off before servicing either unit internally.
note: - The receiver is safe when its supplies are switched off at the Supply Unit. The supply unit is completely safe only when isolated from the mains,

### 7.2.1 Valve Renlacements

The valve types used in the receiver and their functions are listed in Table 5. Valve feeds should be checked periodically as described in Section 7.4.3.1 and a record should be kept. Any valve whose feed is below the minimum specified in Table 8 should be renewed.

NOTE: - For these routine checks it is not necessary to measure valve feeds under all the conditions shown in I'able 8; the feeds should be measured with the UF GAIN control at maximum and the operational switch set to CH. MAN (pos. 6).

TABLE 5
List of Valve Types

| Qty | Circuit Ref. | Type | Functions |
| :---: | :---: | :--- | :--- |
| 2 | V1, V2 | CV. 138 Pentode <br> Marconi Z.77 (6AM6) | Signal Frequency Anglifier |
| 1 | V3 | CV.453 Heptode <br> Marconi X.77 (6BE6) | First Mixer |
| 1 | V4 | CV.453 Heptode <br> Marconi X.77 (6BE6) | Second Mixer |

TABLE 5 (Cont'd)

| Qty | Circuit Ref. | Type | Functions |
| :---: | :---: | :--- | :--- |
| 2 | V5, V6 | CV.131 Pentode <br> Marconi W. 77 | Intermediate Frequency Amplifier |
| 1 | V7 | CV.452 Double- <br> Diode -triode <br> Marconi DH. 77 (6AT6) | Detector, AGC rectifier and AF <br> Amplifier |
| 1 | V8 | CV.133 Triode <br> Marconi L. 77 (6C4) | Audio Frequency Output |
| 1 | V9 | CV.452 Double-diode - <br> Triode <br> Marconi DH. 77 (6AT6) | Noise Limiter and Calibrating <br> Oscillator |
| 1 | V10 | CV.138 Pentode <br> Marconi Z.77 (6AM6) | Crystal First Oscillator |
| 1 | V11 | CV.138 Pentode <br> Marconi Z. 77 (6AM6) | Variable LC First Oscillator |
| 1 | V12 | CV.133 Triode <br> Marconi L. 77 (6C4) | Second Oscillator |
| 1 | V13 | CV.131 Pentode <br> Marconi W. 77 | Third (beat) Oscillator |
| 1 | V14 | CV. 287 <br> Marconi QS. 150/15 | Voltage Stabiliser |

### 7.2.2 Renewing the Calibration Drum Drive Cord (See Fig. s)

(a) Remove receiver from case.
(b) Remove all control knobs and disconnect meter.
(c) Remove front panel.
(d) Replace temporarily the band switch control knob and set the switch to BAND 4.
(c) Check that the rotors of this switch are correctly set to band 4.
(f) Remove the right-hand drum support bracket and cheek; withdraw the calibrated drum from the left-hand cheek $A$.
(g) Take 6 feet of cord, bring ends together and fold double. Pass loop through on periphery of cheek $A$ and tie a knot near the end of the loop so that it is retained.
(h) Take one end (call this the LH cord). Pass this cord straight down over pulley $B$, then on to pulleys $C$ and $D$ and around the large-diameter drive pulley $E$ to the hole in its periphery.
(i) Take the other end (call this the RH cord) $1^{1 / 2}$ times around cheek $A$, then down to pulleys $G$ and $F$ and around to the hole in the drive pulley $E$.
(j) Pass both ends of the cord through the hole in $E$ and secure them to the end of the spring so that it is in tension.

### 7.2.3 Replacing the Pointer Brive Cord

(a) Set the 0-25 logging scale at 3.
(b) Release pointer from cord and pull cord out through inspection hole in the front plate of drive, but do not detach from spring.
(c) Thread new cord, which should be 44 inches long, through pointer slider and pass ends around the drum, the right-hand end clockwise and left-hand end counter-clockwise. Tuck the cord ends through the hole in the periphery of the drum; there should now be approximately $11 / 2$ turns of cord on the drum.
(d) Pull cord back through hole in drum thus extending the spring, and ease cord over small pulleys at each end of pulley guide.
(e) Secure pointer lightly to cord so that the pointer is at the middle of scale when logging scale is at 12.5.
(f) Check position of pointer on calibration scale by tuning receiver to a station of known frequency near the middle of scale. Secure pointer firmly to cord, taking care not to cut it.
(g) Replace front panel and control knobs.

### 7.3 CIRCUIT CHECKS

In the event of a receiver failure not due to valves or fuses, endeavour to narrow down the possible causes by a logical sequence of tests. For example, a failure observable on only one of the frequency bands would exonerate IF and AF circuits; a failure which occurs only when the passband switch set to $1 \mathrm{kc} / \mathrm{s}$ passband would probably be due to the crystal filter.

If the possible cause of a fault is localised in this manner the fault may often be traced by resistance checks using an Avometer or similar measuring instrument.

## 7. 4 VOLTAGES AND FEEDS

A model 7 Avometer or other similar type of instrument should be used for measuring voltages and feeds. The receiver should have its full complement of valves and lamps; the links should be connected across the AGC and desensitising terminals. Unless otherwise stated, the receiver controls should be set as follows:-

Band Change switch (SWA) to BAND 1.
Passband Switch (SWB) to $1 \mathrm{kc} / \mathrm{s}$.

Operational Switch (SWC) to CW-MAN.
Meter Switch (SWD) to blank position (position 12)
First Oscillator Selector (SWE) to VARIABLE.
HF gain control (RV.93, RV94) to maximum (fully clockwise)
The measured values of current and voltage should be within the limits specified in Tables 6 to 10 when the mains input to the Supply Unit Type $1325 / 4$ (or $1325 / 5$ ) is 230 Volts.
7.4.1

TABLE 6
Power Consumption

| HT current $=$ |  |
| :--- | :--- |
| LT current $=$ | 50 to 80 mA at 280 V <br> 2.6 to 4.0 A at $6.3 \mathrm{~V}, 50 \mathrm{c} / \mathrm{s}$ |

7.4 .2

TABLE 7
Vol tages
(Voltages are measured on a Model 7 Avometer or other instrument of 500 ohms per volt)

| Test | Test Points | Meter Range | voltages |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | hF gain max. | HF gain min. |
| HT Voltage | Supplies plug (PLA) <br> pin 4 and chassis | 400 V | 2.50 to 310V | 265 to 330V |
| Stabilised HT voltage | V14, pin 5 and chassis | 400 V | 140 to 160 V | 140 to 160 V |
| Heater voltage | Supplies plug (PLA) <br> pins 1 and 7 and chassis | 10V | 5.6 to 7.0 V | 5.6 to 7.0 V |
| RF Cathode 1 ine | Slider of Rv94 (rear unit of HF gain control) and chassis | 100 V | 0 | 2.8 to 4.2V |
| IF Cathode line | Slider of RV93 (front unit of HF gain control) and chassis | 100 V | 0 | 16 to 24 V |

### 7.4.3 Valve Feeds

### 7.4.3.1 Metered Feeds

These valve feeds are measured on the meter incorporated in the receiver and should be within the limits specified in Table 8.

TABLE 8

| Mater Switch position | Operational Switch position | HF gain to Max. Reading ${ }_{\mathrm{HF}} \mathrm{gain}$ to Min. |  |
| :---: | :---: | :---: | :---: |
| V1 | $\begin{array}{r} 1-3,5,6 \\ 4,7 \\ \hline \end{array}$ | $\begin{gathered} 1.8 \text { to } 3.6 \\ 0 \end{gathered}$ | $\begin{gathered} 0.2 \text { to } 0.5 \\ 0 \end{gathered}$ |
| V2 | $\begin{gathered} 1-3,5-7 \\ 4 \\ \hline \end{gathered}$ | $\begin{gathered} 1.8 \text { to } 3.6 \\ 0 \end{gathered}$ | $\begin{gathered} 0.2 \text { to } 0.5 \\ 0 \end{gathered}$ |
| V3 | $\begin{gathered} 1-3,5-7 \\ 4 \end{gathered}$ | $\begin{gathered} 1.5 \text { to } 3.0 \\ 0 \end{gathered}$ | $\begin{gathered} 1.7 \text { to } 3.4 \\ 0 \end{gathered}$ |
| V4 | $\begin{gathered} 1-3,5-7 \\ 4 \\ \hline \end{gathered}$ | $\begin{gathered} 1.3 \text { to } 2.6 \\ 0 \end{gathered}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ |
| V5 | $\begin{gathered} 1-3,5-7 \\ 4 \\ \hline \end{gathered}$ | $\begin{aligned} & 3.5 \text { to } 5.3 \\ & 4.0 \text { to } 6.0 \end{aligned}$ | $\begin{aligned} & 0.4 \text { to } 0.8 \\ & 2.2 \text { to } 3.4 \end{aligned}$ |
| V6 | $\begin{gathered} 1,3,5-7 \\ 4 \\ \hline \end{gathered}$ | $\begin{gathered} 5.8 \text { to } 8.8 \\ 0 \end{gathered}$ | $\begin{gathered} 6.4 \text { to } 9.7 \\ 0 \end{gathered}$ |
| (a) V 10 | $\begin{gathered} 1.3,5-7 \\ 4 \end{gathered}$ | $\begin{aligned} & 2.4 \text { to } 3.6 \\ & 2.9 \text { to } 4.3 \end{aligned}$ | $\begin{aligned} & 4.5 \text { to } 4.0 \\ & 3.0 \text { to } 4.5 \end{aligned}$ |
| V11 | 1-7 | 3.7 to 5.7 | 3.7 to 5.7 |
| V12 | 1-7 | 0.7 to 1.1 | 0.5 to 0.9 |
| V13 | $\begin{aligned} & 1-4 \\ & 5-7 \end{aligned}$ | $\begin{gathered} 0 \\ 1.6 \text { to } 2.6 \end{gathered}$ | $\begin{gathered} 0 \\ 1.6 \text { to } 2.6 \end{gathered}$ |

(a) With first oscillator selector switch to XL1. No crystal.

### 7.4.3.2 Feeds to V7 and V8

The feeds to V7 and V8 are checked by measuring the cathode voltages on the 100 volt range of the model 7 Avometer. These should be within the limits specified in Table 9.

TABLE 9

| Test points | operational Switch <br> position | Vol tage |
| :--- | :---: | :---: |
| V7 to pin 2 <br> and chassis | $1-3,5-7$ | 12 to 18 V |
| V8 to pin 7 <br> and chassis | $1-3,5-7$ | 14 to 21 V |
| 4.5 to 14 V |  |  |
| 10 to 16 V |  |  |

### 7.4.3.3 Feed to v9

The feed to the calibrator valve v9 is measured by setting the operational switch to CW-MAN. and connecting the Avometer ( 10 mA range) between supplies plug PLA, Pin 4 and SHC1.R tag 8 (this tag is mounted on the rear side of the front wafer of the operational switch). If the cathode (pin 2) of $v 9$ is then earthed, the feed to v9 may
be read and should be 0.8 to 1.2 mA when the anode inductor L 24 is tuned for minimum feed.

### 7.4.3.4 Current Through Staliliser Tube (V14)

The current through V14 is measured by connecting the Avometer in the load between pins 1, 2 and 3 of V14 and chassis. The current through V14 should be within the limits specified in Table 10.

TABLE 10

| operational Switch <br> position | current |
| :---: | :---: |
| $1-3,5-7$ | 4.0 to 6.0 mA |
| 4 | 7.0 to 11.0 mA |

### 7.5 RECEIVER RE-ALIGNMENT

Unless otherwise stated all controls should be set as for Section 7.4; one of the aerial sockets should be short-circuited.

### 7.5. 1 Test Equipment

(a) Signal generator(s) covering the range 0.45 to $32 \mathrm{Mc} / \mathrm{s}$ and having a maximum output of not less than 1 volt in series with 75 ohms.
(b) One alignment oscilloscope (Samwell and Hutton Type 43 B , specify crystal frequency of $465 \mathrm{kc} / \mathrm{s}$.
(c) One tone generator covering the range 100 to $6000 \mathrm{c} / \mathrm{s}$ and having a maximum output of not less than 5 volts in series with 600 ohms.
(d) One valve-voltmeter (Marconi Instrument Type TF. 428B).
(e) One AF output meter to measure 0.1 to 100 mW in impedances of 3 and 600 and 5000 ohms (Marconi Instrument Type TF. 340A).
(f) One dummy load resistor, 600 ohms $\pm 5 \%, 1 / 2$ watt.
(g) One capacitor $0.1 \mu \mathrm{~F}, 350$ volt working, fitted with crocodile clips.
(h) One signal generator output lead fitted with signal generator and AM plugs and having a 68 ohm series resistor.
(j) One $100 \mu \mathrm{~A}$ meter.
(k) One trimming tool type W. $8201 / \mathrm{C}$ Sh. 1 Ed. A. (mounted in spring clips on receiver chassis).
(1) One damping resistor 10,000 ohms $\pm 20 \%$ \%att.
(m) One damping resistor 1,000 ohms $\pm 20 \% ~ 1 / 4$ watt.

### 7.5.2 AF amplifier Tests

Set the AF GAIN control to its mid-position.

### 7.5.2.1 Sensitivity

(a) Connect the 3 ohm output meter across the loudspeaker output terminals (LS).
(b) Apply an input at $400 \mathrm{c} / \mathrm{s}$ through the $0.1 \mu \mathrm{~F}$ capacitor to the grid of V 8 (pin 1).
(c) The input required for 50 mW ( +17 dbm ) output into 3 ohms should be 3.8 to 5.8 volts.
(d) Transfer the input to the slider of the AF gain control (RV92). The input required for $50 \mathrm{~m} / \mathrm{W}$ output into 3 ohms should be 0.10 to 0.16 volts. Check that the relation between output and input is linear for output levels less than 100 m .
(e) Transfer the output meter to the 600 ohm line output terminals. The input to the AF gain control to obtain an output of 10 mW ( +10 dbm ) into 600 ohms should be 0.10 to 0.16 volts.
(f) Transfer the output meter to one of the phones jacks. The input to the AF gain control for 1 mW ( 0 dbm ) output into 5000 ohms should be 0.08 to 0.14 volts. Repeat for the other phones jack.

### 7.5.2.2 Frequency Response

(a) Connect the 600 ohm dummy load to the line output terminals and connect the valve-vol tmeter across it.
(b) Apply input at $1000 \mathrm{c} / \mathrm{s}$ through $0.1 \mu \mathrm{~F}$ to the top of the AF gain control and set the input level to give 1.00 volts output into 600 ohms. The total variation in frequency response between 100 and $6000 \mathrm{c} / \mathrm{s}$ should not exceed 1.5db.

### 7.5.3 Alignment of $465 \mathrm{kc} / \mathrm{s}$ IF Amplifier Circuits

### 7.5.3.1 General

The complete alignment of the IF circuits incorporating crystal filters is impossible without a suitable alignment oscilloscope and should only be undertaken by skilled servicing staff. The alignment oscilloscope has been designed specially for this purpose, and the method of using it is described in Section 7.5.3.5. When no such oscilloscope is available, only the $8 \mathrm{kc} / \mathrm{s}$ and $13 \mathrm{kc} . \mathrm{s}$ band-pass filters should be re-aligned using the procedure described in Sections 7.5.3.6; it is most unlikely that IF circuits thus re-aligned would be fully satisfactory on the crystal-controlled passbands ( $3 \mathrm{kc} / \mathrm{s}$ and $1 \mathrm{kc} / \mathrm{s}$ ) and, therefore adjustments should not be undertaken unless absolutely necessary.

### 7.5.3.2 Controls

Set the operational switch to MOD. - MAN and the HF gain control to maximum; other controls as for Section 7.4.

### 7.5.3.3 Tuning IPT.4, IFT. 5 and IFT. 6 (without alignment oscilloscope)

(a) Set the passband switch to $1 \mathrm{kc} / \mathrm{s}$. Apply a modulated signal at $465 \mathrm{kc} / \mathrm{s}$ to V4 at the junction of R25 and R28 and tune the signal to the crystal filter (i.e. for maximum output).
(b) Set the passband switch to $8 \mathrm{kc} / \mathrm{s}$ and apply the signal to V6 (SWB. 4.2). Adjust the upper and lower cores of IFT. 6 for maximum output.
(c) Apply the signal to V5 (SWB. 2. 1) and connect the 10 kilohm damping resistor across the primary of IPT. 4 (V5 pin 5 and C53). Adjust the trimmer capacitor C57 for maximum output.
(d) Set the passband switch to $13 \mathrm{kc} / \mathrm{s}$ and adjust the trimmer C126 for maximum output. Transfer the damping resistor to the secondary of IFT.4, (SWB4 tag 11 and chassis) and adjust the lower core of IFT. 4 for maximum output. Remove the damping resistor.
NOTE: - The settings of the upper cores of IFT. 4 and IFT. 5 and the capacitance trimmer in IFT. 5 should not be disturbed.

### 7.5.3.4 Tuning IFT. 4, IFT. 5 and IFT. 6 (with alignment oscilloscope)

(a) Check that the Operational switch is set to Mod. - MAN and the HF GAIN control to near maximum.
(b) Set the passband switch to $1 \mathrm{kc} / \mathrm{s}$. Apply a modulated signal at $465 \mathrm{kc} / \mathrm{s}$ to V4, (junction of R25 and R28) and tune it to the crystal filter. Adjust the cores in IFT. 6, IFT. 5, IFw.4, IFT. 3 and IFT. 2 for maximum output. Disconnect the signal generator.
(c) Connect the amplifier input of the alignment oscilloscope to the signal diode (V7 pin 5) through a 1 to 2 pF capacitor. Connect the IF output from the alignment oscilloscope to V5 grid (SWB2. 1).
(d) Using the logarithmic display, adjust the two cores in IFT. 4 and the core in IFT. 5 until the response is greatest near the crystal resonant frequencies which are seen as sharp peaks and dips in the response.

(e) Adjust the crystal balancing capacitor C58 at the top of IFT. 5 until the two dips appear on either side of the main response. These dips should be moved out until the return humps $A$ in the sketch below are at least $20 d b$ below the main response B. Adjust the cores in IFT. 4 and IFT. 5 until the centre peak is as bigh and as wide as possible; the upper cores of these transformers will have the greatest effect on the bandwidth.
(f) Set the passband switch to $8 \mathrm{kc} / \mathrm{s}$ and connect the 10 kilohm damping resistor across the secondard of IFT. 4 (S欮4 tag 11 and chassis). Adjust both cores in IFT. 6 and the lower core only in IFT. 4 for maximum response at the midband frequency of the $1 \mathrm{kc} / \mathrm{s}$ crystal filter. Remove the damping resistor and adjust the capacitance trimmer C57 for a response symmetrical about this mid-band frequency.
(g) Set the passband switch to $13 \mathrm{kc} / \mathrm{s}$ and adjust the trimmer C 126 for a response symmetrical about the mid-band frequency of the $1 \mathrm{kc} / \mathrm{s}$ filter.
(h) Set the passband switch to $1 \mathrm{kc} / \mathrm{s}$ and check that the response of the crystal filter is satisfactory; if necessary adjust the upper core of IFT. 5 and the balancing capacitor C58.

### 7.5.3.5 Third 0scillator

## Tuning

(a) With unmodulated input to V5 at the midband frequency of the crystal filter as for Section 7.5.3.3, set the operational switch to CW-MAN. and the third oscillator tuning capacitor c118 to its mid-position which should correspond to half-capacitance (C118 is mounted at the top of the third oscillator can).
(b) Adjust the core in the third oscillator screening can for zero beat between the third oscillator and the applied signal.

### 7.5.3.5 Third Oscillator, Tuning and Output Voltage

(a) Connect the valve-voltmeter between pin 2 of the third oscillator anode inductor (L31) and chassis. Tune L31 for maximum output on the meter; this output voltage should be greater than 50 volts.
(b) Disconnect the valve-voltmeter. Adjust the third oscillator tuning capacitor (C118) so that the beat note between the $465 \mathrm{kc} / \mathrm{s}$ signal applied as above and the third oscillator is approximately $1 \mathrm{kc} / \mathrm{s}$; tune L31 for maximum AF output at this frequency.
(c) Connect the $100 \mu \mathrm{~A}$ meter in series with the detector load resistor R 49 and check that the third oscillator produces a detector current greater than $40 \mu \mathrm{~A}$.
(d) Disconnect the microammeter and set the operational switch to MOD, - MAN.

### 7.5.3.6 Tuning IFT. 2 and IFT. 3 (without alignment oscilloscope)

(a) Set the passband switch to $8 \mathrm{kc} / \mathrm{s}$ and apply the modulated signal at $465 \mathrm{kc} / \mathrm{s}$, tuned to the crystal filter as for Section 7.5.3.3 to V4 (junction of R25 and R28).
(b) Connect the 10 kilohm damping resistor across the primary of IFT. 2 (V4, pin 5 and C42), and adjust the trimmer C47 for maximum output.
(c) Set the passband switch to $13 \mathrm{kc} / \mathrm{s}$ and adjust the trimmer Cl24 for maximum output.
(d) Transfer the damping resistor the secondary of IFT. 2 (SWB2, tag 11 and chassis), and adjust the lower core of IFT. 2 for maximum output. Remove the damping resistor.
NOTE: - The settings of the upper cores in IFT, 2 and IFT, 3 and the capacitance trimmer in IFT. 3 should not be disturbed.

### 7.5.3.7 Tuning IFT. 2 and IFT. 3 (with alignment oscilloscope)

(a) Set the passband switch to $3 \mathrm{kc} / \mathrm{s}$.
(b) Connect the IF output of the alignment oscilloscope to $V 4$ grid (junction of R25 and R28).
(c) Tune IFT. 2 and IFT. 3 using the procedure described in Section 7.5.3.4.
(d) Set the passband switch to $8 \mathrm{kc} / \mathrm{s}$ and connect the 10 kilohm damping resistor across IFT. 2 secondary (SHE2. 11 and chassis).
(e) Adjust the lower core in IFT. 2 for maximum response at the mid-band frequency of the $1 \mathrm{kc} / \mathrm{s}$ crystal filter. Remove the damping resistor and adjust the capacitance trismer C47 for a response symmetrical about this mid-band frequency.
(f) Set the passband switch to $13 \mathrm{kc} / \mathrm{s}$ and adjust the trimmer C124 for a symmetrical response.
(g) Set the passband switch to $3 \mathrm{kc} / \mathrm{s}$ and check that the response of the crystal filter is satisfactory, if necessary adjusting the upper core of IFT. 3 and the balancing capacitor C48.

### 7.5.3.8 Capacitance Trimmers C47, C124 C57 and $\mathbf{C 1 2 6}$

These trimmers are connected in parallel with fixed capacitors C46, C123, C56 and C125 respectively. If the minimura capacitance of any one of these combinations is too great to allow the circuit to be tuned with the trimer, then the fixed capacitor should be disconnected.

### 7.5.3.9 Retuning IFT. 6 (after using alignment oscilloscope)

(a) Disconnect the oscilloscope amplifier from the signal diode. Connect the $100 \mu$ A meter in series with the diode load resistor R49.
(b) Apply input to $V 4$ at the mid-band frequency of the $1 \mathrm{kc} / \mathrm{s}$ crystal filter and adjust the upper (secondary) core of IFT. 6 for maximum meter reading,

### 7.5.4 Secoind Oscillator

Tuning
(a) Set the IF passband switch to $1 \mathrm{kc} / \mathrm{s}$.
(b) Set the fine-tuning control (C102 to zero; this should correspond to its half-capacitance position.
(c) Set the signal generator to $1600 \pm 1 \mathrm{kc} / \mathrm{s}$ and connect it through a $0.1 \mu \mathrm{~F}$ capacitance to $V 4$ (junction of R25 and R28).
(d) Adjust the core in the second oscillator screening can for maximum IF output indicated on the microammeter.

## Output Voltages

Connect the valve-voltmeter between the oscillator grid (pin 1) of V4 and chassis; the second oscillator voltage at this point should be 6 to 12 volts.

### 7.5.5 Selectivity of $465 \mathrm{kc} / \mathrm{s}$ IF Amplifier

The bandwidths of the $465 \mathrm{kc} / \mathrm{s}$ IF amplifier at 6 db and at 40 db below maximum for the four positions of the passband switch should be as shown in Table 11.

TABLE 11
Amplifier Selectivity

| Switch Position | Passbands |  |
| :--- | :--- | :--- |
|  | -6dt |  |
| $1 \mathrm{kc} / \mathrm{s}$ | Greater than $700 \mathrm{c} / \mathrm{s}$ | Less than $5000 \mathrm{c} / \mathrm{s}$ |
| $3 \mathrm{kc} / \mathrm{s}$ | Greater than $2500 \mathrm{c} / \mathrm{s}$ | Less than $10,000 \mathrm{c} / \mathrm{s}$ |
| $8 \mathrm{kc} / \mathrm{s}$ | Greater than $7000 \mathrm{c} / \mathrm{s}$ | Less than $20.000 \mathrm{c} / \mathrm{s}$ |
| $13 \mathrm{kc} / \mathrm{s}$ | Greater than $12.500 \mathrm{c} / \mathrm{s}$ | Less than $33,000 \mathrm{c} / \mathrm{s}$ |

### 7.5.6 Stage Gains of $465 \mathrm{kc} / \mathrm{s}$ IF Amplifier

Before measuring the stage gains of the $465 \mathrm{kc} / \mathrm{s}$ IF amplifier the controls should be adjusted as follows:-
(a) Set the HF and AF gain controls to maximum.
(b) Set the Operational Switch to CW-MAN.
(c) Set the IF passband switch to $8 \mathrm{kc} / \mathrm{s}$.
(d) Set the third oscillator tuning capacitor for $1 \mathrm{kc} / \mathrm{s}$ beat note (as in Section 7.5.3.5).
(e) Connect the 3 ohm output meter to the LS terminals,
(f) Set up the signal generator at $465 \mathrm{kc} / \mathrm{s}$ to the mid-band frequency of the 1 kc/s crystal filter.
(g) Connect the signal generator output through a $0,1 \mu F$ capacitor to the control grids of $V 6, V_{5}$ and $V 4$ in turn; measure the inputs required to give 50 mH output into 3 ohns. These inputs should be within the limits shown in Table 12.

TABLE 12
$465 \mathrm{kc} / \mathrm{s}$ Stage Gains

| Input at $465 \mathrm{kc} / \mathrm{s}$ to $V 6 \mathrm{grid}$ for 50 mW | $87-93 \mathrm{db}$ rel. $1 \mu \mathrm{~V}$ |
| :--- | :--- |
| Input at $465 \mathrm{kc} / \mathrm{s}$ to V 5 grid for 50 mW | $52-58 \mathrm{db}$ rel. $1 \mu \mathrm{~N}$ |
| Input at $465 \mathrm{kc} / \mathrm{s}$ to $V 4$ grid for 50 mW | $26-32 \mathrm{db}$ rel. $1 \mu \mathrm{~V}$ |

(h) Apply input at $1600 \mathrm{kc} / \mathrm{s}$ through a $0.1 \mu$ F capacitor to $V 4$ control grid; the input for 50 mW output into 3 ohms should be 27 - 33db relative to 1 microvolt.

### 7.5.7 Variation of Gain with Bandwidth

Controls to be set as for Section 7.5.6.
(a) Apply $465 \mathrm{kc} / \mathrm{s}$ input to V 4 control grid at the mid-band frequency of the $1 \mathrm{kc} / \mathrm{s}$ crystal filter.
(b) Measure the input required to give 50 mW output into 3 ohms for each of the four IF bandwidths; these inputs should be within the limits specified in Table 13.

TABLE 13
Variation of Gain with Bandwidth

| IF Bandwidth | Input at $465 \mathrm{kc} / \mathrm{s}$ to v4 for 50 mW output |
| :---: | :---: |
| $1 \mathrm{kc} / \mathrm{s}$ | $28-34 \mathrm{db}$ relative to $1 \mu \mathrm{~V}$ |
| $3 \mathrm{kc} / \mathrm{s}$ | $26-32 \mathrm{db}$ relative to $1 \mu \mathrm{~V}$ |
| $8 \mathrm{kc} / \mathrm{s}$ | $26-32 \mathrm{db}$ relative to $1 \mu \mathrm{~V}$ |
| $13 \mathrm{kc} / \mathrm{s}$ | $35-41 \mathrm{db}$ relative to $1 \mu N$ |

### 7.5.8 $1600 \mathrm{kc} / \mathrm{s}$ IF Amplifier

Set the receiver controls as follows:-
(a) Band change switch (SWA) to Band 1
(b) Tuning control to $2 \mathrm{mc} / \mathrm{s}$.
(c) First Oscillator switch (SWE) to VAR. OSC.
(d) Operational switch to MOD. - MAN.
(e) IF pass band switch to $8 \mathrm{kc} / \mathrm{s}$.
(f) $\mathrm{HF}^{\mathrm{F}}$ gain control to minimum.

### 7.5.8.1 IF. 1 Response

(a) Using the valve-voltmeter, check that the RF voltage across the oscillator (front) section of the ganged tuning capacitors is 12 to 28 volts.
(b) Connect the VVM between V4 grid (junction of R25 and R28) and chassis.
(c) Tune the signal generator to $1600 \mathrm{kc} / \mathrm{s}$ and connect its output through a $0.1 \mu \mathrm{~F}$ capacitor to V 3 grid (junction of R17 and R18).
(d) Adjust both cores of IFT. 1 for maximum output on the VVM.
(e) Connect the 10 kilohm damping resistor across the primary (between anode of V3, pin 5 and C35). Readjust the upper (secondary) core for maximum output.
(f) Remove the 10 kilohm resistor; connect a 1000 ohms damping resistor across the VVM and adjust the lower (primary) core for maximura output. Remove the damping resistor.
(g) Adjust the input level so that the output at $1600 \mathrm{kc} / \mathrm{s}$ is 1 volt. Measure the response of IF. 1 on the VVM , maintaining the input level constant; the total variation in response over the band $1600 \mathrm{kc} / \mathrm{s} \pm 10 \mathrm{kc} / \mathrm{s}$ should be less than 1 db .

### 7.5.8.2 Retuning IFT. 1

(a) Remove the valve-voltmeter.
(b) Set the IF passband switch to $1 \mathrm{kc} / \mathrm{s}$.
(c) Set the fine-tuning control to zero,
(d) Set the operational switch to CH-MAN.
(e) Apply input at $1600 \mathrm{kc} / \mathrm{s}$ to V 3 and adjust the input frequency for maximum output.
(f) Connect the 10 kilohm damping resistor across the primary of IFT, 1 and adjust the secondary (upper) core for maximum output. Remove the damping resistor.

### 7.5.8.3 IF. 1 Gain

(a) Set the $H F$ and $A F$ gain controls to maximum.
(b) Set the operational switch to CW-MAN.
(c) Set the IF passband switch to $8 \mathrm{kc} / \mathrm{s}$.
(d) Set the fine-tuning control to zero.
(e) Apply unmodulated input at $1600 \mathrm{kc} / \mathrm{s}$ through a $0.1 \mu \mathrm{~F}$ capacitor to V3 grid (junction of R17 and R18); measure the input required to give 50 mW output
into 3 ohms; the input should be 12 to 18 db relative to 1 microvolt.
(f) Repeat this measurement with input at $2 \mathrm{Mc} / \mathrm{s}$; this input should be 18 to 24db relative to 1 microvolt.

### 7.5.9 Signal Frequency Amplifier

### 7.5.9.1 First Oscillator Alignment

(a) Set the bandchange switch to Band 4.
(b) Set the first oscillator selector to VAR. OSC.
(c) Set the passband switch to $3 \mathrm{kc} / \mathrm{s}$.
(d) Set the operational switch to CW-MAN.
(e) Apply input at $8 \mathrm{mc} / \mathrm{s}$ from the signal generator to V3 (junction of $R 17$ and R18) through a $0.1 / \boldsymbol{F}$ capacitor.
(f) Set the tuning pointer to the $16 \mathrm{Mc} / \mathrm{s}$ calibration mark and adjust the core of Band 4 oscillator coil (L26) for zero beat.
(g) Set the input frequency and tuning pointer to $32.00 \mathrm{Mc} / \mathrm{s}$ and adjust the penny plate capacitor $\mathbf{C 9 8}(\mathrm{b})$ (See Fig. 7 upper deck plan) for zero beat. Do not under any circumstances alter the compensating capacitor C98(a). Repeat this procedure until the oscillator frequency corresponds with the printed calibration marks at 16 and $32 \mathrm{Mc} / \mathrm{s}$.
(h) Set the bandchange switch to Band 3. Set the input frequency and pointer to $8 \mathrm{Mc} / \mathrm{s}$ and adjust the core of Band 3 oscillator coil (L27) for zero beat. Check that the calibration is approximately correct at $16 \mathrm{Mc} / \mathrm{s}$.
(i) Set the bandchange switch to Band 2. Set the input frequency and pointer to $4 \mathrm{Mc} / \mathrm{s}$ and adjust the core of Band 2 oscillator coil (L28) for zero beat. Set the input frequency and pointer to $8 \mathrm{Mc} / \mathrm{s}$ and adjust the capacitance trimmer Cl30 for zero beat. Repeat this procedure until the oscillator frequency corresponds with the calibration marks at $4 \mathrm{Mc} / \mathrm{s}$ and $8 \mathrm{Mc} / \mathrm{s}$.
(j) Set the bandchange switch to Band 1 and repeat the procedure at 2 and at $4 \mathrm{Mc} / \mathrm{s}$, adjusting the core of $L 29$ and capacitor $\mathbf{C 9 7}$.

### 7.5.9.2 Alignment of Signal Frequency Circuits

(a) Connect the signal generator through a 68 ohm resistor to one aerial socket and short circuit the other aerial socket.
(b) Set the bandchange switch to Band 1 and the tuning pointer to $2 \mathrm{Mc} / \mathrm{s}$. Tune the signal generator (at $2 \mathrm{mc} / \mathrm{s}$ ) to the receiver. Adjust the cores in the mixer (L12), HF(L8) and the aerial (L4) coils on band 1 for maximum receiver output.
(c) Set the signal generator to $4.0 \mathrm{Mc} / \mathrm{s}$ and tune in the signal at the high frequency end of Band 1. Adjust the capacitance trimmers C27, C14 and C4.
(d) Repeat the adjustments of the inductor coils at the LF end of the band and the capacitance trimaers at the $H F$ and until no further improvement in ganging is obtained.
(e) Gang the receiver in a similar manner on Bands 2 and 3.
(f) On Band 4, set the passband switch to $13 \mathrm{kc} / \mathrm{s}$ and then gang as before, taking care to retune the receiver oscillator after every adjustment of the trimmers in the SF amplifier.

### 7.5. 10 First Oscillator Voltages

### 7.5.10.1 Variable LC 0scillator

Connect the valve-voltmeter across the oscillator section of the gang capacitor and measure the oscillator voltages throughout each band; these voltages should be within the limits specified in Table 14.

TABLE 14
Variable first Oscillator Voltage

| Band | Frequency in Mc/s | Vol tages |
| :---: | :---: | :---: |
| 1 | $2-44$ | $15-35$ |
| 2 | $4-88$ | $12-30$ |
| 3 | $8-16$ | $10-25$ |
| 4 | $16-32$ | $6-14$ |

### 7.5.10.2 Crystal Oscillator

(a) Set the first oscillator selector switch to XL. 1.
(b) Connect the valve-voltmeter across the oscillator section of the gang capacitor.
(c) Set the band switch and tuning control to the corresponding signal frequency and adjust the tuning for maximum output on the VVM.
(d) Repeat this procedure for the other five crystals; the voltages measured on the VVM should be within the limits shown in Table 15.

TABLE 15
Crystal Oscillator Voltages

| Band | 1 | 2 | 3 | 4 |
| :--- | :---: | :---: | :---: | :---: |
| Output in Volts | $15-45$ | $12-36$ | $10-30$ | $5-15$ |

### 7.5.10.3 External Oscillator

(a) Set the first oscillator selector switch to EXT.OSC.
(b) Connect the VVM across the temperature compensator.
(c) Connect the signal generator through a 68 ohm resistor to the external oscillator Pye plug at the rear of the receiver.
(d) Set the receiver tuning to $2 \mathrm{Mc} / \mathrm{s}$ and tune the signal generator at $3.6 \mathrm{Mc} / \mathrm{s}$ for maximum output on the VVM.
(e) Measure the input for 1 volt output on the WVM.
(f) Repeat this measurement at the frequencies shown in Table 16; the inputs, in series with 78 ohms, required to give 1 volt output should be within the limits specified.

TABLE 16
External Oscillator Inputs

| Band | Signal Frequency in $\mathrm{Mc} / \mathrm{s}$ | Input Frequency in Mc/s | Input in do rel. $1 \mu \mathrm{~V}$ in series with 78 ohms. |
| :---: | :---: | :---: | :---: |
| 1 | 2.0 | 3.6 | 100-106 |
|  | 4.0 | 5.6 | 98-104 |
| 2 | 4.0 | 5.6 | 101-107 |
|  | 8.0 | 9.6 | 99-105 |
| 3 | 8.0 | 9.6 | 101-107 |
|  | 16.0 | 17.6 | 100-106 |
| 4 | 16.0 | 17.6 | $103-109$ |
|  | 32.0 | 33.6 | $100-106$ |

## 7. 6 OVERALL PERFORMANCE

Set the passband switch to $8 \mathrm{kc} / \mathrm{s}$.

### 7.6.1 CTS Sensitivity

The nominal input. in series with 75 ohms required to give 20db signal-to-noise ratio is given in column 3 of Table 17.

### 7.6.2 Sensitivity for Modulated Signals

With the signal generator modulated $40 \%$ at $400 \mathrm{c} / \mathrm{s}$, the nominal input in series With 75 ohms required to give 10 db signal-to-noise ratio is given in column 3 of Table 17.

### 7.6.3 AGC

The increase in output when the signal is increased by 60 db above the sensitivity figures given in Table 17 should not be more than 10 db .

### 7.6.4 Inage Protection

The nominal attenuation offered to the image signal is given in column 4 of Table 17.

TABLE 17

| Performance |  |  |  |
| :---: | :---: | :---: | :---: |
| Band | Frequency <br> in Mc/s | Sensitivity <br> (dD re). $1 \mu V)$ | Image Protection <br> in $d \mathrm{~b}$ |
| 1 | 2 | 3 | 110 |
|  | 3 | 4 | 100 |
|  | 4 | 5 | 90 |
| 2 | 4 | 3 | 110 |
|  | 6 | 4 | 100 |
|  | 8 | 5 | 90 |
| 3 | 8 | 3 | 100 |
|  | 12 | 4 | 85 |
|  | 16 | 5 | 70 |
| 4 | 16 | 6 | 85 |
|  | 24 | 5 | 65 |
|  | 32 | 9 | 50 |

### 7.7 ADDITIONAL PERFORHANCE DATA

### 7.7.1 Stage Gains of Signal Frequency Amplifier

(a) Set the operational switch to CW-MAN
(b) Connect the slider of the rear section (RV.94) of the HF gain control to earth so that, for this test, control is applied only to the IF valves.
(c) The input to the aerial socket ismeasured with the signal generator in series with 68 ohms; the inputs to the valve grids are measured with the signal generator in series with $0,1 \mu \mathrm{~F}$. The nominal stage gains should be as shown in Table 18.

TABLE 18
Nominal SF Stage Gains

| Band | Frequency <br> Mc/s | Voltage gain in decibels |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $V_{1}$ to V2 | $V 2$ to V3 |  |
| 1 | 2 | 19 | 16 | 6 |
|  | 3 | 20 | 7 | 9 |
|  | 4 | 20 | 2 | 10 |
| 2 | 4 | 17 | 12 | 6 |
|  | 6 | 18 | 6 | 11 |
|  | 8 | 19 | 2 | 13 |

T. 27 19/1 6974

TABLE 18 (Cont'd)

| Band | Frequency in $\mathrm{Mc} / \mathrm{s}$ | Voltage gain in decibels |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Aerial to V1 | V1 to V2 | V2 20 V 3 |
| 3 | 8 | 14 | 16 | 9 |
|  | 12 | 14 | 10 | 11 |
|  | 16 | 15 | 8 | 14 |
| 4 | 16 | 9 | 16 | 18 |
|  | 24 | 9 | 9 | 21 |
|  | 32 | 9 | 6 | 18 |

### 7.7.2 Selectivity of SF Amplifier

The attenuation of the image signal is a measure of the selectivity of the SF stages. It is measured with the input applied to $V 1$ and $V 2$ grids through a $0.1 \mu \mathrm{~F}$ capacitor and to the aerial through 68 ohms.

The nominal image signal protection in db is shown in Table 19.

TABLE 19

| Band | Frequency in Mc/s | Image protection in decibels |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { Input to } \mathrm{V} 2 \\ \text { Grid } \end{gathered}$ | $\begin{gathered} \text { Moput to } V I \\ \text { Grid } \end{gathered}$ | $\begin{aligned} & \text { Input to } \\ & \text { aerial } \end{aligned}$ |
| 1 | 2 | 25 | 72 | 110 |
|  | 3 | 25 | 70 | 100 |
|  | 4 | 25 | 62 | 90 |
| 2 | 4 | 35 | 76 | 110 |
|  | 6 | 35 | 66 | 100 |
|  | 8 | 35 | 58 | 90 |
| 3 | 8 | 35 | 64 | 100 |
|  | 12 | 32 | 58 | 85 |
|  | 16 | 27 | 48 | 70 |
| 4 | 16 | 25 | 62 | 85 |
|  | 24 | 19 | 50 | 65 |
|  | 32 | 15 | 35 | 50 |

### 7.7.3 SJ Amplifier Detune Ratios

(a) Set the IF passband switch to $8 \mathrm{kc} / \mathrm{s}$.
(b) Set the operational switch to CW-MAN.
(c) Set the HF gain control to maximum.
(d) Disconnect the signal generator from the aerial socket so that the receiver input circuit is not loaded by the aerial impedance.
(e) Adjust the ureial trimmer capacitor for maximum noise output. Note this output and then short-circuit V grid to chassis through a $0.1 \mu \mathrm{~F}$ capacitor and again note the output; the reduction in noise output in decibels is the detune ratio and the nominal values are shown in Table 20.

TABLE 20
SF Amplifier Detune Ratios

| Band | 1 | 2 | 3 | 4 |
| :--- | :--- | :--- | :--- | :--- |
| Detune Ratio <br> (db) | 9 | 8 | 6 | 5 |

(f) Apply input at 78 ohms impedance to the aerial socket and reset the capacitance trimmers in the aerial circuit for maximum output at $4,8,16$ and $32 \mathrm{Mc} / \mathrm{s}$.

### 7.8 SUPPLY UNIT

The voltages measured across the output terminals of the supply unit with no load and wi th the receiver load (HT $=65 \mathrm{~mA}, \mathrm{LT}=3.7 \mathrm{~A}$ ) should be within the limits shown in Table 21. The ripple voltage should not exceed $0.1 \%$.

TABLE 21
Supply Unit Outputs

|  | With no load | Witn receiver load |
| :--- | :--- | :--- |
| HT Volts | $370-470 \mathrm{~V}$ | $250-310 \mathrm{~V}$ |
| LT Volts | 6.6 volts AC $\pm 10 \%$ | 6.3 volts AC $\pm 10 \%$ |

## 8 USEFUL AUXIALIARY EQUIPMENT

At locations where a number of receivers are installed it is usually desirable to equip the station with a set of instruments for routine performance checks and realignment. The list of apparatus included in Table 22 is a brief guide to suitable items for this purpose. The Marconi Instrument Co. Ltd., catalogue gives performance figures of all types of instrument manufactured by that Company.

TABLE 22
Test Apparatus

| Apparatus | Marconi Instruments <br> Type |
| :--- | :---: |
| Signal Generator <br> $15 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ |  |
| Beat Frequency Oscillator | TF. 867 |
| Audio Power Meter | TF. 195 L |

## 9 COMPONENTS \& SPARES

### 9.1 MALN ITEMS

The equipment comprises two of the three main units listed in Table 23.

TABLE 23

| Unit | Type No. |
| :---: | :---: |
| Receiver | CR. 150/6 |
| Supply Unit <br> Or <br> Supply Unit | $1325 / 4$ |

### 9.2 ACCESSORIES

These are loose items, other than valves, which are included with the main items 1isted in Table 23.

TABLE 24
Accessories

| Qty | Description | Identity |
| :---: | :--- | :--- |
| 1 | Connector Assembly (Supply Unit to <br> Receiver) | WZ.3956/C Sh. I |
| 2 | Connector (Supply Unit to Mains) | WIS.3206/C Sh. 1 |
| 2 | Plugs (Aerial input) | W. 6015/A Ref.72 |
| 1 | Socket (Ext. Oscillator input) | W. 6015/A Ref. 227 |
| 1 | Socket (465 kc/s output) | W. 6015/A Ref.227 |
| 1 | Trimming Tool | W. 8201/C Sh.1 Ed.B |

NOTE: - When the receivers and supply units are mounted in a cabinet or rack, the external connectors are part of the cableform supplied with the equipment.

### 9.3 COMPONENTS LIST

Receiver Type CR150/6
No. 1
Supply Unit Type 1325/4)
Supply Unit Type 1325/5
No. 2

## COMPONENTS LIST No. 1 <br> FOR

HF. COMMUNICATIONS RECEIVER TYPE CR. 150/6
(Drg. No. W.35074)

## NOTES

1. When ordering spares quote information from all columns for identities marked * or identity only for all other items.
2. The references in column 1 are shown on circuit diagram, Fig. 6 and component location diagram, Fig. 7.
3. For identical items the total quantity is given at the first entry.

| Item No. | $\begin{aligned} & \text { Unit } \\ & \text { No. } \end{aligned}$ | Gircuit Ref. | Dastription | $\begin{gathered} \text { Value } \\ \text { and } \\ \text { Tolerance } \end{gathered}$ | Rating Watts, Working Volesge DC, etc. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | capacitors |  |  |  |
| 1 |  | C1 | Air Dielectric Trimmer | 3-30pF | 75 V | WSK. 13605/16 |
| 2 |  | c2 | Air Dielectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | WSK. 13605/15 |
| 3 |  | C3 | Air Dielectric Trimmer | $3-30 \mathrm{pF}$ | 75 V | MSK. 13605/14 |
| 4 |  | C4 | Air Diel ectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | PC. 18801/10 |
| 5 |  | C5 | Moul ded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | WSK. 13605/19 |
| 6 |  | c6 | Ceramic | 5pF $\pm 20 \%$ | 750 V | W. 36827/38 |
|  |  | c7 | Ceramic | $5 \mathrm{pF} \pm 20 \%$ | 750V | WSK. 13607/42 |
| 8 |  |  |  |  |  |  |
|  |  | c9 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801/10 |
| 10 |  | C10 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801/10 |
| 11 |  | c11 | Ceramic | $5 \mathrm{pF} \pm 20 \%$ | 750v | H. $36827 / 38$ |
| 12 |  |  |  |  |  |  |
| 13 |  | C13 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801/10 |
| 14 |  | C14 | Air Diel ectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | HSK. 13607/14 |
| 15 |  | C15 | Air Diel ectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | HSK. 13607/13 |
| 16 |  | C16 | Air Diel ectric | 3-30pF | 75V | WSK. 13607/12 |


| Item No. | Unit No. | Gircuit Ref. | Description | $\begin{gathered} \text { Value } \\ \text { and } \\ \text { Tolerance } \end{gathered}$ | Rating <br> Watts, <br> Working <br> Voltage DC, te. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | CAPACITORS (Cont* d) |  |  |  |
| 17 |  | C17 | Air Dielectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | WSK. 13607/11 |
| 18 |  | C18 | Silver Mica | $10 \mathrm{pF} \pm 10 \%$ | 350 V | WSK. 13607/20 |
| 19 |  | C19 | Silver Mica | $100 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18702/1 |
| 20 |  | C20 | Silver Mica | $220 \mathrm{pF} \pm 5 \%$ | 750V | PC. 18802/17 |
| 21 |  | C21 | Silver Mica | . $002 \mu \mathrm{~F} \pm 5$ \% | 350 V | HSK. 13607/18 |
| 22 |  | C 22 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801/10 |
| 23 |  | C23 | Moul ded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350V | PC. 18801/10 |
| 24 |  | C 24 | Air Dielectric Trimmer | $3-30 \mathrm{pF}$ | 75V | WSK. 13606/13 |
| 25 |  | C25 | Air Dielectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | WSK. 13606/14 |
| 26 |  | C26 | Air Dielectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | HSk. 13606/15 |
| 27 |  | C27 | Air Dielectric Trimer | 3-30pF | 75 V | WSK. 13606/16 |
| 28 | . | C28 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801/10 |
| 29 |  | C29 | Ceramic | $5 \mathrm{pF} \pm 20 \%$ | 350 V | W. 36827/38 |
| 30 |  | C30 | Silver Mica | $100 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/13 |
| 31 |  | C31 | Ceramic | 100pF $\pm 20 \%$ | 350 V | PC. 18202/13 |
| 32 |  | C32 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 460 V | PC. 18801/10 |
| 33 |  | C33 | Silver Mica | 10pF $\pm 10 \%$ | 350 V | WSK. 13608/39 |
| 34 |  | C34 | Moulded Mica | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801/10 |
| 35 |  | C35 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 15 \%$ | 350V | W. 36677/B/3 |
| 36 |  | C36 | Silver Mica | $100 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/13 |
| 37 |  | C37 | Silver Mica | $22 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/5 |
| 38 |  | C38 | Paper Tubular | . $02 \mu \mathrm{~F} \pm 20 \%$ | 350 V | W. 35074/12 |
| 39 |  | C39 | Paper Tubular | . $1 \mu \mathbf{F} \pm 20 \%$ | 1000 V | W. 35074/9 |
| 40 |  | C40 | Silver Mica | $470 \mathrm{pF} \pm 20 \%$ | 350 V | PC. 18802 21 |
| 41 |  | C41 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000V | W. 35074/9 |
| 42 |  | C42 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | W. 35074/9 |
| 43 |  | C43 | Silver Mica | $220 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/17 |
| 44 |  | C44 | Silver Mica | $180 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/16 |
| 45 |  | C45 | Paper Tubular | . $02 \mu \mathrm{~F} \pm 20 \%$ | 350 V | W. 35074/1/12 |
| 46 |  | C46 | Silver Mica | $20 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/5 |
| 47 |  | C47 | Air Dielectric Trimmer | 3-30pF | 75 V | W. 36666/14 |


| Item No. | Unit Na . | Circuit Ref. | Description | $\begin{aligned} & \text { Value } \\ & \text { and } \\ & \text { Tolerance } \end{aligned}$ | Rating <br> Watts. <br> Working <br> Voltage DC. etc. | GA. No./Re\%. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | CAPACITGIS (Con |  |  |  |
| 48 |  | C48 | Trimmer | 2-8pF | 75 V | W. 20048/B/15 |
| 49 |  | C49 | Ceramic | 6. $8 \mathrm{pFF} \pm 10 \%$ | 350 V | WV. 20048/B/3 |
| 50 |  | C50 | Silver Mica | $56 \mathrm{pF} \pm 5 \%$ | 350 V | W. 20048/B/16 |
| 51 |  | C51 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | W. 35074/15 |
| 52 |  | C52 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | H. 35074/9 |
| 53 |  | C53 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000V | W. 35074/9 |
| 54 |  | C54 | Silver Mica | $220 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/17 |
| 55 |  | C55 | Silver Mica | 180pF $\pm 5 \%$ | 350 V | PC. 18802/16 |
| 56 |  | C56 | Silver Mica | 20pF $\pm 5 \%$ | 350 V | PC. 18802/5 |
| 57 |  | C57 | Air Dielectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75V | W. 36666/15 |
| 58 |  | C58 | Trimmer | 2-8pF | 75 V | W. 20048/B/3 |
| 59 |  | C59 | Ceramic | $6.8 \mathrm{pF} \pm 10 \%$ | 350 V | PC. $18201^{\prime} 7$ |
| 60 |  | C60 | Silver Mica | $56 \mathrm{pF} \pm 5 \%$ | 350 V | W. 20048/B/15 |
| 61 |  | C61 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | W. 35074/9 |
| 62 |  | C62 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | W. 35074/9 |
| 63 |  | C63 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | W. 35074/9 |
| 64 |  | C64 | Moulded Mica | $100 \mathrm{pF} \pm 20 \%$ | 350 V | PC. 18802/13 |
| 65 |  | C65 | Moul ded Mica | 100pF $\pm 20 \%$ | 350 V | PC. 18702/1 |
| 66 |  | C66 | Paper Tubular | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/9 |
| 67 |  | C67 | Silver Mica | $180 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/16 |
| 68 |  | C68 | Silver Mica | $220 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/17 |
| 69 |  | C69 | Ceramic | $2 \mathrm{pF} \pm 20 \%$ | 350 V | PC. 18201/3 |
| 70 |  | C70 | Moul ded Mica | 100pF $\pm 20 \%$ | 350 V | PC. 18702/1 |
| 71 |  | C71 | Moul ded Mica | 100pF $\pm 20 \%$ | 350 V | PC. 18702/1 |
| 72 |  | C72 | Paper Tubular | . $1 \mu \mathrm{~F}+20 \%$ | 1000 V | W. 35074/9 |
| 73 |  | C73 | Paper Tubular | $1 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/20 |
| 74 |  | 074 | Paper Tubular | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/9 |
| 75 |  | C75 | El ectrolytic | $25 \mu \mathrm{~F}$ | 25 V | PC. 18402/12 |
| 76 |  | C76 | Silver Mica | $500 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18702/4 |
| 77 |  | C77 | Paper Tubular | . $01 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/9 |
| 78 |  | C78 | El ectrolytic | $25 /{ }^{\text {F }}$ | 25 V | PC. 18402 '15 |
| 79 |  | C79 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/14 |
| 80 |  | C80 | Moul ded Mica | . $001 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 18801 / |
| 81 |  | C81 | Silver Mica | $200 \mathrm{pF} \pm 5 \%$ | 350 V | WSK. 13289/16 |
| 82 |  | C82 | Silver Mica | $1000 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18801/4 |
| 83 |  | C83 | Ceramic | 1pF $\pm 50 \%$ | 350 V | PC. $18201 / 1$ |


| Item No. | Unit No. | Circuit Ref. | Description | Value and Tolerance | Rating <br> Watts. <br> Working <br> Voltage DC, etc. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | CAPACITORS (Cont' d) |  |  |  |
| 84 |  | C84 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000V | W. 36827/36 |
| 85 |  | C85 | Paper Tubular | $.1 \mu F \pm 20 \%$ | 1000 V | W. 36827/36 |
| 86 |  | C86 | Ceramic | 100pF $\pm 20 \%$ | 350 V | PC. $18202 / 13$ |
| 87 |  | C87 | Silver Mica | $47 \mathrm{pF} \pm 20 \%$ | 350 V | W. $36827 / 48$ |
| 88 |  | C88 | Ceramic | $47 \mathrm{pF} \pm 20 \%$ | 350 V | PC. 18201/17 |
| 89 |  | C89 | Moulded Mica | $500 \mathrm{pF} \pm 20 \%$ | 350V | PC. 18702/4 |
| 90 |  | $\mathrm{C9O}$ | Ceramic | 100pF $\pm 10 \%$ | 350 V | PC. 18202/13 |
| 91 |  |  |  |  |  |  |
| 92 |  | C92 | Ceramic | $100 \mathrm{pF} \pm 10 \%$ | 350 V | PC. 18202/13 |
| 93 |  | C93 | Silver Mica | $1700 \mathrm{pF} \pm 15 \%$ | 350 V | MSK. 13608/14 |
| 94 |  | 094 | Silver Mica | $890 \mathrm{pF} \pm 10 \%$ | 350 V | WSK. 13608/15 |
| 95 |  | 69 | Silver Mica | $480 \mathrm{pF} \pm 5 \%$ | 350 V | HSK. 13608/16 |
| 96 |  | C96 | Silver Mica | $263 \mathrm{pF} \pm 5 \%$ | 350 V | WSK, 13608/17 |
| 97 |  | C97 | Air Dielectric Trimmer |  |  |  |
| 98 |  | C98 | Trimmer ${ }^{\text {Temperature Comp. }}$ | 3-30pF | 75 V | HSK. 13608/44 <br> W. 36827/1/24 |
| 99 |  |  |  |  |  |  |
| 100 |  | C100 | Silver Mica | $220 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/17 |
| 101 |  | C101 | Silver Mica | $500 \mathrm{pF} \pm 5 \%$ | 350V | HSK. 13160/15 |
| 102 |  | C102 | Trimmer | 10pp |  | HSK. 13160/10 |
| 103 |  | C103 | Silver Mica | 2000pF $\pm 5 \%$ | 350 V | WFK. 13160/17 |
| 104 |  | C104 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000 V | W. 35074/9 |
| 105 |  | C105 | Paper Tubular | . $1 \mu \mathrm{FF} \pm 20 \%$ | 1000 V | H. 35074/9 |
| 106 |  | C106 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 1000V | W. 35074/9 |
| 107 |  | C107 | Paper Tubular | . $5 \mu \mathrm{~F} \pm 25 \%$ | 150V | PC. 19301/3 |
| 108 |  | C108 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/14 |
| 109 |  | C109 | Paper Tubular | . $02 \mu \mathrm{~F} \pm 20 \%$ | 350 V | F. 35074/12 |
| 110 |  | C110 | Paper Tubular |  | 1000 V | W. 35074/9 |
| 111 |  | C111 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 350 V | PC. 19202/14 |
| 112 |  | C112 | Paper Tubular | . $1 \mu \mathrm{~F}$ 土20\% | 350V | PC. 19202/14 |
| 113 |  | C113 | Paper Tubular | . $1 \mu \mathrm{~F} \pm 20 \%$ | 350V | PC. 19202/14 |
| 114 |  | C114 | Moulded Mica | $470 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/21 |
| 115 |  | C115 | Silver Mica | $100 \mathrm{pF} \pm 5 \%$ | 350 V | PC. 18802/13 |
| 116 |  | C116 | Silver Mica | 420pF $\pm 5 \%$ | 350 V | WSK, 13161/12 |
| 117 |  | C117 | Silver Mica | $2000 \mathrm{pF} \pm 5 \%$ | 350 V | HSK. 13161/13 |
| 118 |  | C118 | Trimmer | 10 pF |  | WSK. 14161/8 |


| Item No. | Unit No. | Circuit Ref. | Description | Value and Tolerance | Rating <br> Watts, <br> Working <br> Voltage DC. atc. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Caraciturs (Cont' d) |  |  |  |
| 119 |  | C119) |  |  |  |  |
| 120 |  | C120) | 4 Gang Variable |  |  |  |
| 121 |  | C121) | 163.8pF Per |  |  | Y. $36827 / 2$ |
| 122 |  | C122) | Section |  |  |  |
| 123 |  | C123 | Sil ver Mica | $22 \mathrm{pF} \pm 5 \%$ | 750 V | PC. 18802/5 |
| 124 |  | C124 | Air Dielectric |  |  |  |
|  |  |  | Trimmer | 3-30pF | 75 V | W. 36666/15 |
| 125 |  | C125 | Silver Mica | $22 \mathrm{pF} \pm 5 \%$ | 750 V | PC. 18802/5 |
| 126 |  | C126 | Air Dielectric | 3-30pr |  | W. 36666/15 |
| 127 |  |  |  |  |  | W. 36666 |
| 128 |  | C1 28 | Ceramic | 2. $2 \mathrm{pF} \pm 5 \%$ | 500 V | PC. 18201/3 |
| 129 |  | C129 | Ceramic | $4.7 \mathrm{pF} \pm 5 \%$ | 500 V | PC. 18201/5 |
| 130 |  | Cl 30 | Air Dielectric Trimmer | 2-8pF | 75 V | HSK. 13608/43 |
| 131 |  |  |  |  |  |  |
| 132 |  |  |  |  |  |  |
| 133 |  |  |  |  |  |  |
| 134 |  |  |  |  |  |  |
| 135 |  |  |  |  |  |  |
|  |  |  | RESISTORS |  |  |  |
| 136 |  | RI | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 45$ |
| 137 |  | R2 | Carbon | $820 \Omega \pm 5 \%$ | 1/4\% | PC. $66611 / 24$ |
| 138 |  | R3 | Carbon | $6.8 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/35 |
| 139 |  | R4 | Carbon | $22 \Omega \pm 20 \%$ | 1/4W | PC. 66610/5 |
| 140 |  | R5 | Carbon | $330 \Omega \pm 20 \%$ | 1/4W | PC. 66610/19 |
| 141 |  | R6 | Carbon | $150 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/51 |
| 142 |  | R7 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 143 |  | R8 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 144 |  | R 9 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 145 |  | R10 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 146 |  | R11 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/45 |
| 147 |  | R12 | Carbon | $68 \Omega \pm 20 \%$ | 1/4 ${ }^{1}$ | PC. $66610 / 11$ |
| 148 |  | R13 | Carbon | $150 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/51 |
| 149 |  | R14 | Carbon | $330 \Omega \pm 20 \%$ | 1/4 H | PC. 66610/19 |


| Item No. | Unit No. | Circuit Ref. | Description | Value and Tolerance | Rating <br> Watts, <br> Working <br> Voltage DC. atc. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | RESISTORS (Cont' d) |  |  |  |
| 150 |  | R15 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. $66604 / 13$ |
| 151 |  | R16 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4\% | PC. $66610 / 37$ |
| 152 |  | R17 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 153 |  | R18 | Carbon | $22 \Omega \pm 20 \%$ | 1/4W | PC. 66610/5 |
| 154 |  | R19 | Carbon | $22 \Omega \pm 20 \%$ | 1/4W | PC. 66610/5 |
| 155 |  | R20 | Carbon | $22 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/41 |
| 156 |  | R21 | Carbon | $330 \Omega \pm 20 \%$ | 1/4W | PC. 66610/19 |
| 157 |  | R 22 | Carbon | $33 \mathrm{k} \Omega \pm 20 \%$ | 10W | PC. 67010/22 |
| 158 |  | R23 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/3 |
| 159 |  | R24 | Carbon | $22 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 41$ |
| 160 |  | R25 | Carbon | $47 \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 9$ |
| 161 |  | R26 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/45 |
| 162 |  | R27 | Carbon | $47 \Omega \pm 20 \%$ | 1/4\% | PC. 66610/9 |
| 163 |  | R28 | Carbon | $6.8 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/35 |
| 164 |  | R29 | Carbon | $330 \Omega \pm 20 \%$ | 1/4* | PC. $66610 / 19$ |
| 165 |  | R30 | Wirewound Vitreous Enamel | $33 \mathrm{k} \Omega \pm 10 \%$ | $10 \%$ | PC. 67010/22 |
| 166 |  | R31 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 6660413 |
| 167 |  | R32 | Carbon | $22 \mathrm{k} \Omega \pm 20 \%$ | 1/4* | PC. 66610 4 1 |
| 168 |  | R33 | Carbon | $10 \Omega \pm 20 \%$ | 1/4\% | PC. 666101 |
| 169 |  | R34 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4\% | PC. 66610/45 |
| 170 |  | R35 | Carbon | $1 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/25 |
| 171 |  | R36 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 45$ |
| 172 |  | R37 | Carbon | $1 \mathrm{k} \Omega \pm 20 \%$ | 1/4F | PC. 66610/25 |
| 173 |  | R38 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 174 |  | R39 | Carbon | $10 \Omega \pm 20 \%$ | 1/4W | PC. 66610/1 |
| 175 |  | R40 | Carbon | $330 \Omega \pm 20 \%$ | 1/4W | PC. 66610/19 |
| 176 |  | R41 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/45 |
| 177 |  | R42 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 178 |  | R43 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4\% | PC. 66610/37 |
| 179 |  | R44 | Carbon | 220k $\Omega \pm 20 \%$ | 1/4H | PC. 66610/53 |
| $18!$ |  | R45 | Carbon | $150 \mathrm{~K} \Omega \pm 20 \%$ | 1/4W | PC. 66610/57 |
| 81 |  | R46 | Carbon | $330 \mathrm{k} \Omega \pm 20 \%$ | 1/4 H | PC. 66610/55 |
| 182 |  | R47 | Carbon | $1 M \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 61$ |
| 183 |  | R48 | Carbon | $100 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/49 |
| 184 |  | R49 | Carbon | $22 \mathrm{k} \Omega \pm 20 \%$ | 1/47 | PC. $66610 / 41$ |
| 185 |  | R50 | Carbon | $470 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 57$ |


| Item No. | Unit <br> No. | Circuit Ref. | Description | Value <br> Tolerance | Rating <br> Watts, <br> Working <br> Voltage DC. ate. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ReSISTORS (Cont' d) |  |  |  |
| 186 |  | P51 | Carbon | $22 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/41 |
| 187 |  | R52 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/45 |
| 188 |  | R53 | Carbon | $1 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 25$ |
| 189 |  | R54 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 190 |  | R55 | Carbon | $1 M \Omega \pm 20 \%$ | 1/4W | PC. 66610/61 |
| 191 |  | R56 | Carbon | 1. $5 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 27$ |
| 192 |  | R57 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 45$ |
| 193 |  | R58 | Carbon | $4.7 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/33 |
| 194 |  | R59 | Carbon | $100 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 49$ |
| 195 |  | R60 | Carbon | $1 \mathrm{M} \Omega \pm 20 \%$ | 1/4W | PC. 66610/61 |
| 196 |  | R61 | Carbon | $22 k \Omega \pm 20 \%$ | 1/4W | PC. 66610/41 |
| 197 |  | R62 | Carbon | $47 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/45 |
| 198 |  | R63 | Carbon | $68 \mathrm{k} \Omega \pm 20 \%$ | 1/2W | PC. 66611/47 |
| 199 |  | R64 | Carbon | $22 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/41 |
| 200 |  | R65 | Carbon | 47 k ¢ $\pm 20 \%$ | 1/4W | PC. 66610/45 |
| 201 |  | R66 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 202 |  | R67 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 203 |  | R68 | Carbon | $1 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/25 |
| 204 |  | R69 | Carbon | 10\% $\Omega \pm 20 \%$ | IH | $\text { PC. } 66612 / 31$ |
| 205 |  | R70 | Carbon | $22 \Omega \pm 20 \%$ | 1/4 ${ }^{1}$ | PC. 66610/5 |
| 206 |  | R71 | Carbon | $10 \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 1$ |
| 207 |  | R72 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 37$ |
| 208 |  | R73 | Carbon | $22 k \Omega \pm 20 \%$ | 1/4W | PC. 66610/41 |
| 209 |  | R74 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 210 |  | R75 | Carbon | $100 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/49 |
| 211 |  | R76 | Carbon | 2. $2 \mathrm{M} \Omega \pm 10 \%$ | 1/2w | PC. 66610/65 |
| 212 |  | R77 | Carbon | $470 \mathrm{k} \Omega \pm 20 \%$ | 1/4 W | PC. 66610/57 |
| 213 |  | R78 | Carbon | $2.2 \mathrm{M} \sim \pm 20 \%$ | $1 / 4 W$ | PC. 66610/65 |
| 214 |  | R79 | Carbon | $470 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/57 |
| 215 |  | R80 | Carbon | $220 k \Omega \pm 20 \%$ | $1 / 4 \mathrm{~W}$ | PC. 66610/53 |
| 216 |  | R81 | Carbon | $100 \Omega \pm 5 \%$ | 1/4W | PC. 66604/13 |
| 217 |  | R82 | Carbon | 2. $2 k \Omega \pm 20 \%$ | 1/4W | PC. 66610/29 |
| 218 |  | R83 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 219 |  | R84 | Carbon | $100 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/49 |
| 220 |  | R85 | Carbon | $220 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 53$ |
| 221 |  | R86 | Carbon | $820 \Omega \pm 5 \%$ | 1/4W | PC. 66610/24 |
| 222 |  | R87 | Carbon | $14 \mathrm{k} \Omega \pm 5 \%$ | 10W | W. 36679/B/9 |


| Item No. | Unit No. | Circuit Ref. | Deseription | Value and Tolerance | Rating <br> Watts, <br> Working <br> Voltage DC, etc. | GA, No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | RESISTORS (Cont' d) |  |  |  |
| 223 |  | R88 | Carbon | $220 \Omega \pm 20 \%$ | 1/4W | PC. 66610/17 |
| 224 |  | R89 | Carbon | $1 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/25 |
| 225 |  | R290 | Carbon | $1 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. $66610 / 25$ |
| 226 |  | RV9 1 | Variable Linear W. W | $2.5 k \Omega \pm 10 \%$ | 1/2W | PC. 67401 |
| 227 |  | RV92 | Variable Log Law Carbon | 1 M +20\% | 3/8W | PC. 67206/38 |
| 228 |  | RV93 ) | Two Ganged | $2.5 \mathrm{k} \Omega \pm 20 \%$ | 1/2W | W. 35074/6 |
| 229 |  | RV94, | Inverse Law | 2. $5 \mathrm{k} \Omega \pm 20 \%$ | 1/2W | H. 35074/6 |
| 230 |  | RV95 | Variable Linear Carbon | $2.5 \mathrm{k} \Omega \pm 20 \%$ | 3/4W | PC. 67203/5 |
| 231 |  | R96 | Carbon | $10 \mathrm{k} \Omega \pm 20 \%$ | 1/4W | PC. 66610/37 |
| 232 |  | 897 | Carbon | $68 \Omega \pm 20 \%$ | 1/4W | PC. 66610/11 |
| 233 |  | R98 | Carbon | $68 \mathrm{k} \Omega \pm 10 \%$ | 1/2W | PC. 66610/47 |
| 234 |  | R99 | Carbon | $10 \mathrm{k} \Omega \pm 10 \%$ | 1/2 ${ }^{\text {H }}$ | PC. 66610/37 |
| 235 |  | R100 | Carbon | $15 \mathrm{k} \Omega \pm 10 \%$ | 1/2W | PC. 66610 39 |
| 236 |  | R101 | Carbon | $10 \mathrm{k} \Omega \pm 10 \%$ | 1/2W | PC. $66610 / 37$ |
| 237 |  | R102 | Carbon | $15 \mathrm{k} \Omega \pm 10 \%$ | 1/2W | PC. 66610/39 |
| 238 |  | R103 | Carbon | $47 \mathrm{k} \Omega \pm 10 \%$ | 1/2W | PC. $66610 / 45$ |
| 239 |  |  |  |  |  |  |
| 240 |  | R104 | Carbon | $470 \mathrm{k} \Omega \pm 10 \%$ | 1/4W | PC. 66610/21 |
|  |  |  | INDUCTORS |  |  |  |
| 241 |  | L1 | Aerial Section Range 4 |  |  | HSK. 13605/9 |
| 242 |  | L2 | Aerial Section Range 3 |  |  | WSK. 13605/8 |
| 243 |  | L3 | Aerial Section Range 2 |  |  | WSK. 13605/7 |
| 244 |  | L4 | Aerial Section Range 1 |  |  | WSK. 13605/6 |
| 245 |  | L5 | HF Section Range 4 |  |  | WSK. 13607/8 |
| 246 |  | L6 | HF Section Range 3 |  |  | WSK. 13607/6 |
| 247 |  | L7 | HF Section Range 2 |  |  | WSK. 13607/5 |
| 248 |  | L8 | HF Section Range 1 |  |  | WSK. 13607/4 |


| Item No. | Unit No. | Circuit Ref. | Description | Value and Toleranca | Rating <br> Watts. <br> Working <br> Voltage DC. atc. | GA. No./Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 249 250 |  | L9 L10 | Inductors (Cont' d) <br> Mixer Section <br> Range 4 <br> Mixer Section <br> Range 3 |  |  | HSK. 13606/9 <br> HSK. 13606/8 |
| 251 |  | L1 1 | Mixer Section Range 2 |  |  | HSK. 13606/7 |
| 252 |  | L12 | Mixer Section Range 1 |  |  | HSK. 13606/4 |
| 253 |  | L13 | I.F.T. 1 Bottom |  |  | W. 36907/1 |
| 254 |  | LI4 | I. F. T. 1 Top |  |  | W. 36907/1 |
| 255 |  | L15 | I. F. T. 2 Bottom |  |  | W. 16193/B/2 |
| 256 |  | L16 | I.F. T. 2 Top |  |  | W. 16193/B/1 |
| 257 |  | L17 | I.F.T. 3 |  |  | W. 20048/B/1 |
| 258 |  | L18 | I.F. T. 4 Bottom |  |  | W. 16193/B/2 |
| 259 |  | L19 | I.F. T. 4 Top |  |  | W. 16913/B/1 |
| 260 |  | L20 | I. F. T. 5 |  |  | W. 20048/B/1 |
| 261 |  | L21 | Choke |  |  | W. 20039/B/14 |
| 262 |  | L22 | I.F.T. 6 Bottom |  |  | W. 16199/B/2 |
| 263 |  | L23 | I.F.T. 6 Top |  |  | WT. 16199/B/1 |
| 264 |  | L24 | Calibrator |  |  | HSK. 13289/32 |
| 265 |  | L25 | Calibrator |  |  | HSK. 13289/14 |
| 266 |  | L26 | Oscillator <br> Section Range 4 |  |  | MSK. 13608/7 |
| 267 |  | L27 | Oscillator Section Range 3 |  |  | WISK, 13608/6 |
| 268 |  | L28 | Oscillator <br> Section Range 2 |  |  | HSKK. $13608 / 5$ |
| 269 |  | L29 | Oscillator Section Range 1 |  |  | HSK. 13608/4 |
| 270 |  | L30 | 2nd Oscillator |  |  | HSK. 13160/32 |
| 271 |  | L31 | 3rd 0sc. Anode Coil |  |  | W. 35074/24 |
| 272 |  | L32 | Choke |  |  | W. 20039/B/15 |
| 273 |  | L33 | 3rd Oscillator |  |  | W. 13161/18 |
| $\begin{aligned} & 274 \\ & 275 \end{aligned}$ |  |  |  |  |  |  |





## COMPONENTS LIST No. 2

FOR
SUPPLY UNITS TYPE 1325/4 \& 1325/5
(Drg. No. W.35074)

## NOTES

1. When ordering spares quote information from all columns for identities marked * or identity only for all other items.
2. The references in column 1 are shown on circuit diagram, Fig. 8 and component location diagram, Fig. 9.
3. For identical items the total quantity is given at the first entry.




PLACE ELBOW OVER END OF CABLE WITH PROJECTION ON INNER SLEEVE IN ITS KEYWAY G SCREW HOME CAP WITH GUARD:
GLEAN THE CONDU TIGHTEN Grub screw, artar pass through hole in pluc. screw home screen into elbow a
Splay out conductor a SpLAY out conductor a securely soldder as shown. prouecting ends to be trimmed flush
SUITABLE CABLES NOS, is a 19 TELCON AS 42, AS 42M, PTRT, PT 29 M .
100 $\Omega$ UN-RAD10 NO 31, TELCON AS 48 M, PT34, PT34M.



BOTH, ENDS OF CORD PASSED
THROw' END OF SPRING AND
TIED OFF
SIDE VIEW.
FRONT VIEW
SWITCH SHEWN IN FO
ANTICLOCKWISE P
CORD DRIVE ASSEMBLY




## 




UPPERDECK PLAN.







